

Final Report

APPENDIX A: TYPICAL FLOOR LAYOUT



Figure 35: Second Floor Layout of As-Built Building

Final Report

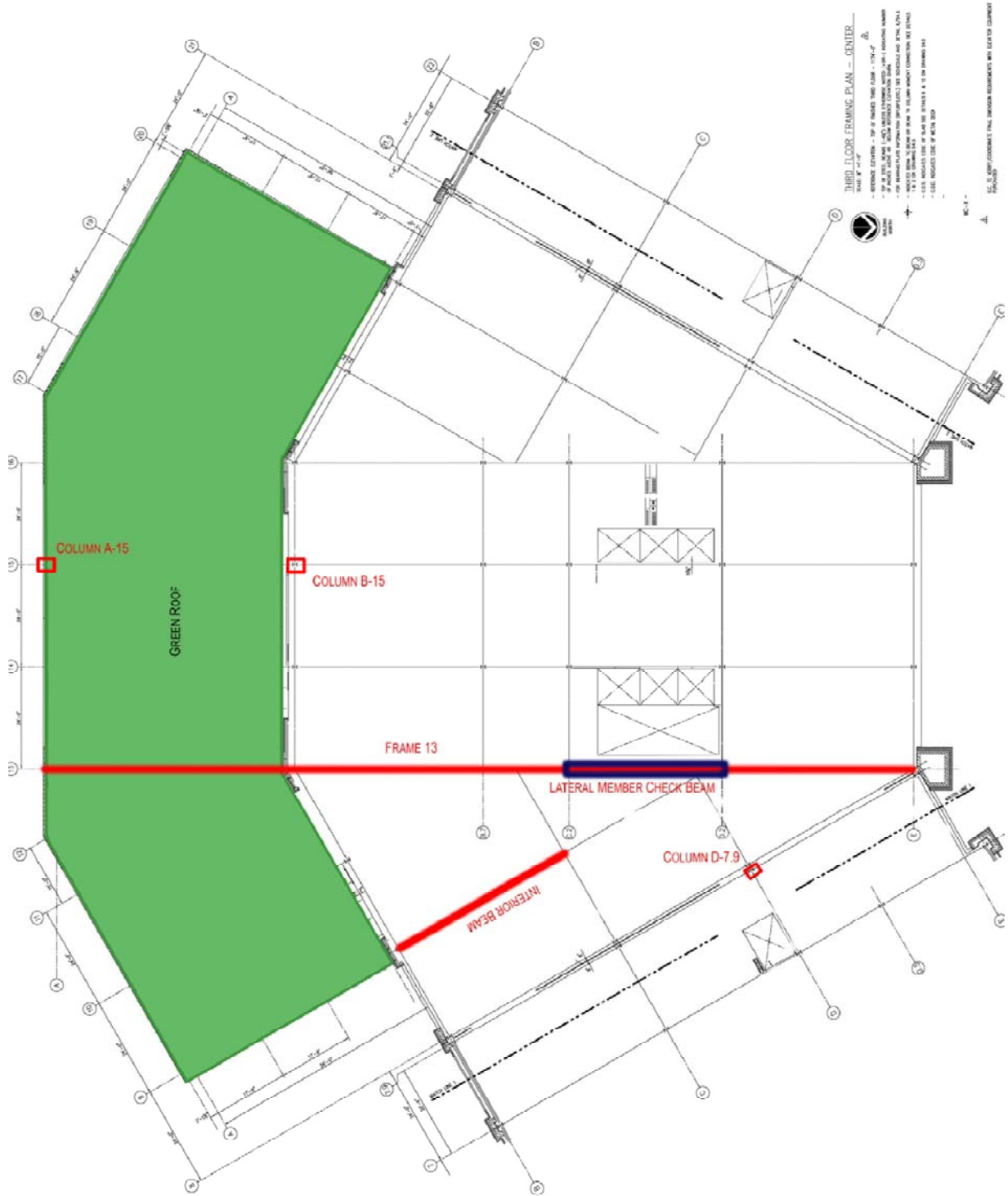


Figure 38: Third Floor Center of Redesigned Concrete Building with Portal Analysis Frame Indicated and Columns for Column Checks Indicated

Final Report

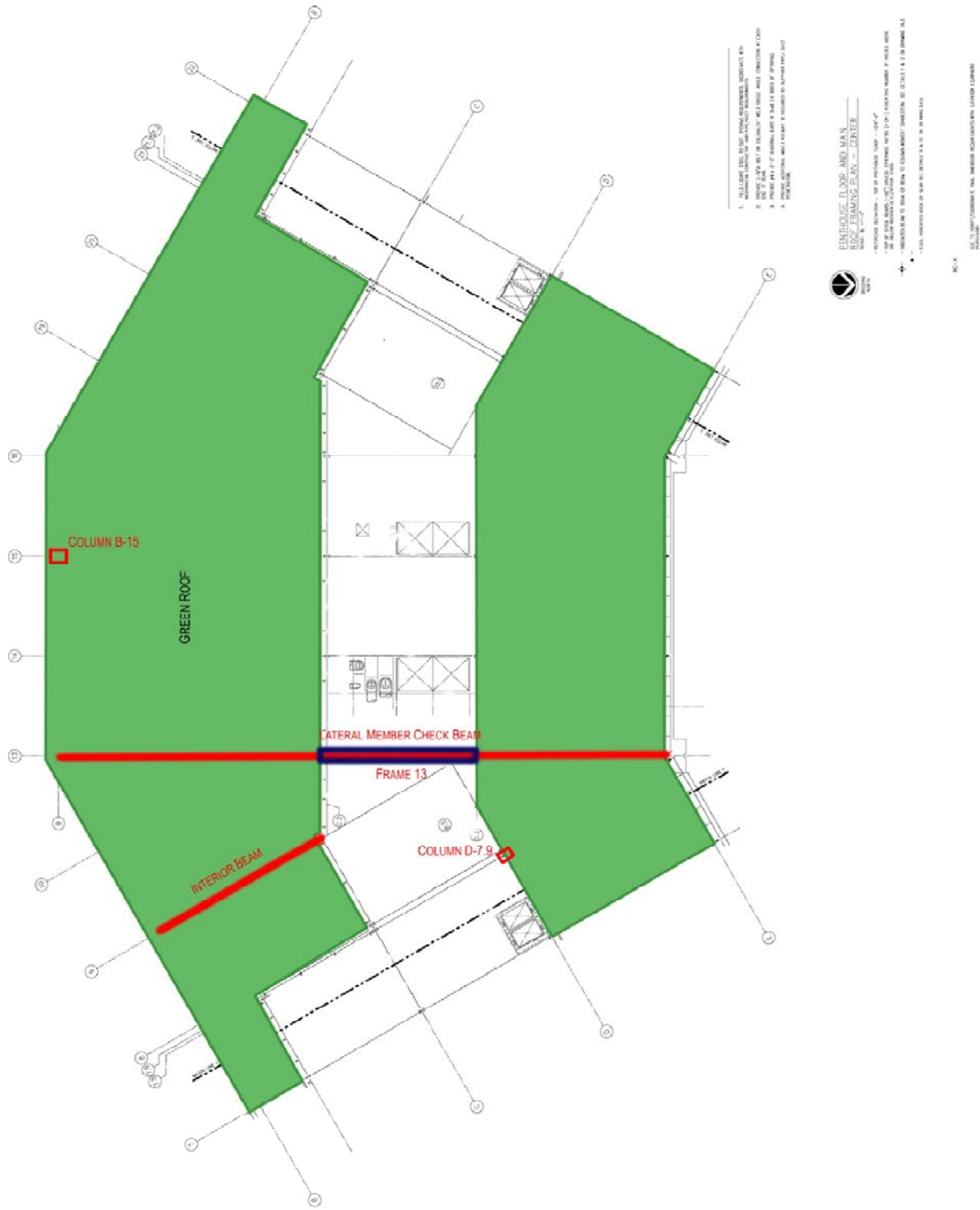


Figure 40: Green Roof Plan Center of Redesigned Building with Portal frame Analysis, lateral Beam Check, Interior Beam Check, and Spot Checked Columns Indicated

APPENDIX B: TORSION EFFECTS CALCULATIONS

The centers of rigidity for each direction were determined by taking the sum of the stiffness in one direction multiplied by the distance from the perpendicular distance from the origin (distance from the opposite origin) all divided by the sum of the stiffness for each frame used in the calculation. For example, the center of rigidity in the Y direction was calculated by taking the K in the X direction and multiplying it by the distance from the Y origin, and finding the sum of all the values divided by the sum of the K's in the X direction ($K_{ix} \cdot d_{ix} / \sum K_{ix}$). The I_x was calculated by taking the sum of the K's in the X direction multiplied by the distance from the Y origin squared ($\sum k_{ix} \cdot y_i^2$). The I_y was calculated using the same method.

$$\text{Center of Rigidity in Y} = K_{ix} \cdot d_{ix} / \sum K_{ix}$$

$$\text{Center of Rigidity in X} = K_{iy} \cdot d_{iy} / \sum K_{iy}$$

$$I_x = \sum k_{ix} \cdot y_i^2$$

$$I_y = \sum k_{iy} \cdot x_i^2$$

After the K values were determined, the K in the direction of the force was divided by the sum of the K's in the same direction and multiplied by the force in the specific direction. The torsion induced moment in each direction was determined differently for wind and for seismic.

For seismic forces, the torsion induced moment was calculated by taking the force at the specified story multiplied by the center of rigidity subtracted from center of mass in the direction perpendicular to the force.

$$\text{Torsion Induced Moment X} = (\text{Force}) \cdot (\text{Center of Mass in Y direction} - \text{Center of Rigidity in X direction})$$

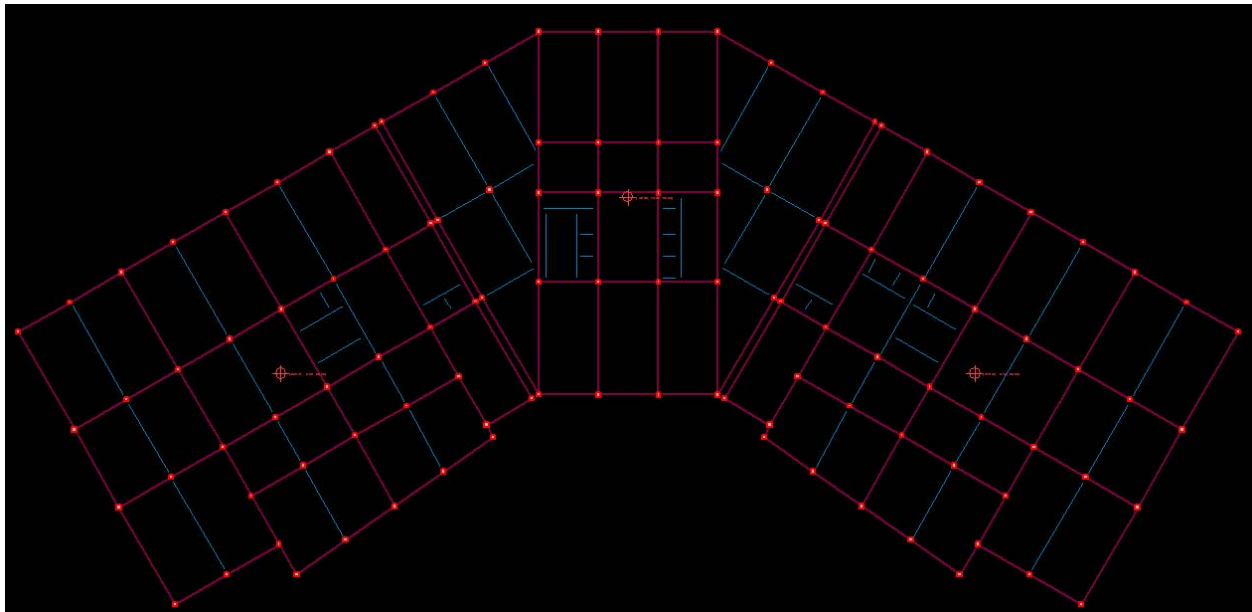


Figure 41: Centers of Mass for New Building

Final Report

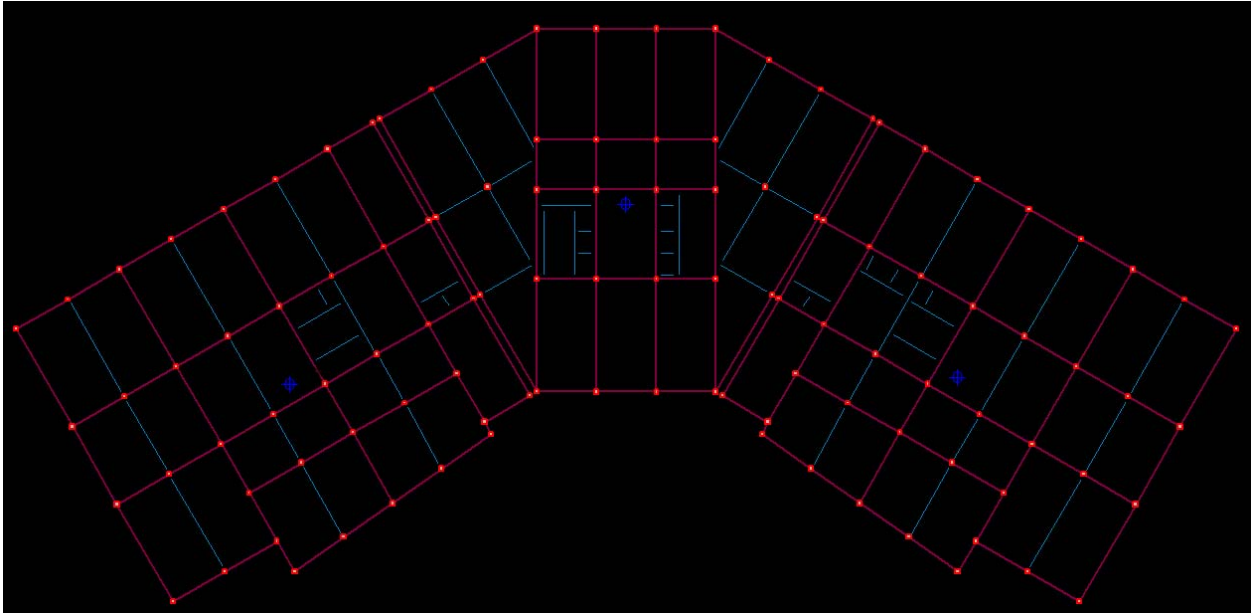


Figure 42: Centers of Rigidity for New Building

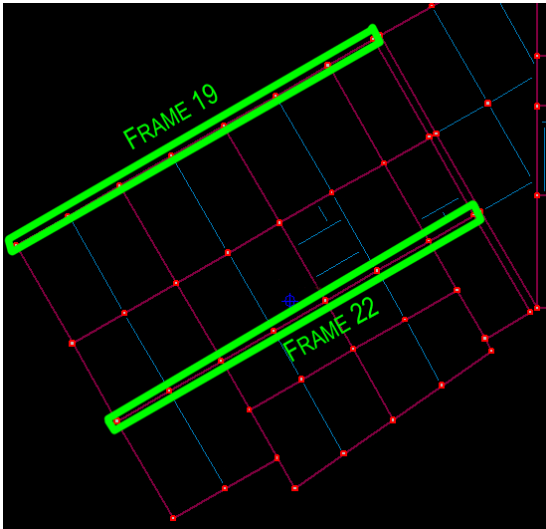


Figure 43: Center of Rigidity and Frames for Comparison

Final Report

As is seen in the following figures of the wind shears from frames 19 and 22, the further away from the center of rigidity the frame is located, the more torsion and shear the frame takes. The concept of torsion is evident in these frames.

Load Case: W9	Wind	Wind IBC06_4_X+Y_CW			
Level		Shear-X kips	Change-X kips	Shear-Y kips	Change-Y kips
Roof		24.27	24.27	17.43	17.43
Fifth		29.05	4.78	20.97	3.54
Fourth		43.42	14.37	31.90	10.93
Third		51.17	7.75	38.22	6.32
Second		46.66	-4.51	33.40	-4.82
First		-9.04	-55.70	-11.12	-44.52

Figure 44: Wind Shears Frame 19

Load Case: W9	Wind	Wind IBC06_4_X+Y_CW			
Level		Shear-X kips	Change-X kips	Shear-Y kips	Change-Y kips
Penthouse		3.26	3.26	3.47	3.47
Roof		3.71	0.45	7.56	4.10
Fifth		9.77	6.06	15.69	8.12
Fourth		12.68	2.91	20.61	4.92
Third		18.67	5.99	27.52	6.92
Second		19.37	0.70	35.57	8.05
First		-3.24	-22.62	-10.30	-45.87

Figure 45: Wind Shears Frame 22

Load Case: E1	Seismic	EQ IBC06_X+E_F			
Level		Shear-X kips	Change-X kips	Shear-Y kips	Change-Y kips
Roof		50.00	50.00	15.85	15.85
Fifth		49.63	-0.37	14.53	-1.33
Fourth		64.72	15.09	19.06	4.54
Third		66.40	1.68	20.10	1.04
Second		73.12	6.72	15.00	-5.10
First		-23.19	-96.31	7.26	-7.74

Figure 46: Seismic Shears Frame 19

Load Case: E1	Seismic	EQ IBC06_X+E_F			
Level		Shear-X kips	Change-X kips	Shear-Y kips	Change-Y kips
Penthouse		20.03	20.03	6.15	6.15
Roof		26.35	6.32	-6.05	-12.20
Fifth		47.99	21.64	-4.00	2.05
Fourth		56.10	8.12	-5.38	-1.38
Third		65.66	9.56	-5.03	0.35
Second		60.39	-5.28	-4.42	0.61
First		-17.19	-77.57	6.33	10.75

Figure 47: Seismic Shears Frame 22

APPENDIX C: WIND LOAD CALCULATIONS

MAIN WIND-FORCE RESISTING SYSTEM (ASCE 7-05)

Table 18: Wind Calculation Conditions

Basic Wind Speed (V) mph	90
Exposure Category	B
Importance Factor (I)	1
Wind Directionality Factor (Kd)	0.85
Topographic Factor (Kzt)	1

BUILDING L/B AND VALUES

Table 19: Windward, Leeward, and Sidewall constants

	L/B	C _p
East-West Direction		
Windward	4.317	0.8
Leeward	4.317	-0.2
Sidewall	4.317	-0.7
North-South Direction		
Windward	0.232	0.8
Leeward	0.232	-0.5
Sidewall	0.232	-0.7

Table 17: Wind Calculation Constants

Variable	Wind Direction	
	N-S	E-W
Stiffness	Flex	Flex
B	544	126
L	126	544
h	92.5	92.5
z	30'	30'
ℓ	320	320
ε	0.333	0.333
α	0.25	0.25
β	0.05	0.05
V	90	90
V _z	67.644	67.644
L _z	380.55	380.55
n ₁	1.163	1.163
N ₁	6.54	6.54
R _n	0.043	0.043
R _h	0.127	0.127
R _b	0.023	0.095
R _L	0.030	0.007
b	0.45	0.45
R	0.037	0.074
l _z	0.275	0.275
g _R	0.000	0.000
q _p	14.836	14.836
g _V	3.4	3.4
Q	0.731	0.832
G _f	0.772	0.830

Final Report

WIND CALCULATIONS CONTINUED:

$$q_p = 0.00256 K_h K_{zt} K_d V^2 I = 14.836$$

$$GC_{pn} = 1.5 \quad -1$$

$$P_p = q_p GC_{pn} = 22.254 \quad -14.836$$

$$n_1 = \frac{43.5}{H^{0.9}} \quad 1.163 \text{ eq (C6-15)}$$

$n_1 > 1$ therefore Rigid structure

$$g_Q = g_V = 3.4$$
$$G = 0.85$$

$$z = 0.6h = 55.5$$

$$z_{\min} = 30'$$

$$I_z = c(33/z)^{1/6} = 0.275$$

$$L_z = l(z/33)^6 = 380.55$$

$$Q_{N-S} = \sqrt{(1/(1+0.63(B+h/L_z)^{0.63}))} = 0.731$$

$$Q_{E-W} = \sqrt{(1/(1+0.63(B+h/L_z)^{0.63}))} = 0.832$$

$$G_{fN-S} = 0.925 [(1+1.7I_z g_Q)/(1+1.7g_V I_z)] = 0.772274$$

$$G_{fE-W} = 0.925 [(1+1.7I_z g_Q)/(1+1.7g_V I_z)] = 0.829674$$

Final Report

WIND CALCULATIONS CONTINUED:

Table 20: Design Wind Pressure in N-S

Design Wind Pressures p in N-S Direction (Table 5.41)						
Location	Height above Ground Level z (ft)	q(psf)	External Pressure qGC_p (psf)	Internal Pressure q_hGC_{pi}	Net Pressure p (psf)	
					+Gcpi	-Gcpi
Windward	92.5	14.354	8.87	2.67	6.20	11.54
	74.5	13.47	8.32	2.67	5.65	10.99
	70	13.20	8.16	2.67	5.49	10.83
	60	12.61	7.79	2.67	5.12	10.46
	50	12.02	7.42	2.67	4.75	10.09
	46	11.72	7.24	2.67	4.57	9.91
	40	11.28	6.97	2.67	4.30	9.64
	32	10.56	6.53	2.67	3.86	9.20
	30	9.79	6.05	2.67	3.38	8.72
	25	9.20	5.68	2.67	3.01	8.35
	20	8.46	5.22	2.67	2.55	7.90
	18	8.46	5.22	2.67	2.55	7.90
	15	8.46	5.22	2.67	2.55	7.90
Leeward	All	14.35	-5.54	2.67	-8.21	-2.87
Side	All	14.35	-7.76	2.67	-10.43	-5.09

Table 21: Design Wind Pressure in E-W

Design Wind Pressures p in E-W Direction (Table 5.41)						
Location	Height above Ground Level z (ft)	q(psf)	External Pressure qGC_p (psf)	Internal Pressure q_hGC_{pi}	Net Pressure p (psf)	
					+Gcpi	-Gcpi
Windward	92.5	14.35	9.53	2.67	6.86	12.20
	74.5	13.47	8.94	2.67	6.27	11.61
	70	13.20	8.76	2.67	6.09	11.43
	60	12.61	8.37	2.67	5.70	11.04
	50	12.02	7.98	2.67	5.31	10.65
	46	11.72	7.78	2.67	5.11	10.45
	40	11.28	7.48	2.67	4.81	10.15
	32	10.56	7.01	2.67	4.34	9.68
	30	10.39	6.89	2.67	4.22	9.56
	25	9.79	6.50	2.67	3.83	9.17
	20	9.20	6.11	2.67	3.43	8.78
	18	8.90	5.91	2.67	3.24	8.58
	15	8.46	5.61	2.67	2.94	8.28
Leeward	All	13.47	-2.24	2.67	-4.91	0.44
Side	All	13.47	-7.82	2.67	-10.49	-5.15

Final Report

WIND CALCULATIONS CONTINUED:

Table 22: Total Wind pressures by Height

Floor Heights	Level	Total Height	K_z	q_z	Wind Pressures (psf)					
					N-S	N-S	N-S	E-W	E-W	E-W
					Windward	Leeward	Side Wall	Windward	Leeward	Sidewall
18	Penthouse	92.5	0.9675	14.354	11.54	-8.21	-10.43	12.20	-4.91	-10.49
14.5	Roof	74.5	0.908	13.471	10.99	-8.21	-10.43	11.61	-4.91	-10.49
14	5	60	0.85	12.611	10.46	-8.21	-10.43	11.43	-4.91	-10.49
14	4	46	0.79	11.720	9.91	-8.21	-10.43	11.04	-4.91	-10.49
14	3	32	0.712	10.563	9.20	-8.21	-10.43	10.65	-4.91	-10.49
18	2	18	0.59	8.902	7.90	-8.21	-10.43	10.45	-4.91	-10.49

Table 23: Wind Forces, Shears, and Moment

Level	Wind Design					
	Load (kips)		Shear (kips)		Moment (ft-k)	
	N-S	E-W	N-S	E-W	N-S	E-W
Pent	193.4	38.8	0	0	3481.3	698.2
Roof	151.5	30.2	193.4	38.8	2196.7	437.6
5	144.8	29.3	344.9	69.0	2026.7	410.7
4	138.0	28.1	489.7	98.3	1932.5	393.8
3	132.6	27.4	627.7	126.4	1856.3	384.1
2	140.2	31.0	760.3	153.9	2523.7	557.2
Total	900.5	184.8	900.5	184.8	10535.9	2183.4

Note: Total Base Shear includes load from Windward and Leeward pressures

Final Report

WIND CALCULATIONS CONTINUED:

RAM COMPARISON

As these tables show, RAM values are around the same change from floor to floor as the hand calculations.

RAM values were compared further to the hand calculation method results used throughout the report and used in previous technical reports. The main differences have already been addressed, such as the possibility of a finite element analysis. The wind design table below is the final story force and story shears for the east portion of the building.

RAM CALCULATED VALUES

Table 24: RAM Calculated Wind Values

Floor Heights	Level	Total Height	K_z	q_z	RAM Wind Pressures (psf)					
					N-S	N-S	N-S	E-W	E-W	E-W
					Windward	Leeward	Side Wall	Windward	Leeward	Sidewall
18	Penthouse	92.5	0.966	14.331	11.57	-8.23	-10.46	11.57	-5.98	-8.23
14.5	Roof	74.5	0.909	13.486	11.05	-8.23	-10.46	11.05	-5.98	-8.23
14	5	60	0.854	12.670	10.54	-8.23	-10.46	10.54	-5.98	-8.23
14	4	46	0.792	11.750	9.97	-8.23	-10.46	9.97	-5.98	-8.23
14	3	32	0.714	10.593	9.25	-8.23	-10.46	9.25	-5.98	-8.23
18	2	18	0.605	8.976	8.25	-8.23	-10.46	8.25	-5.98	-8.23

Table 25: RAM Wind Forces, Shears, and Moments

Level	Wind Design					
	Load (kips)		Shear (kips)		Moment (ft-k)	
	N-S	E-W	N-S	E-W	N-S	E-W
Pent	193.9	39.8	0	0	3491.0	716.6
Roof	152.1	31.1	193.9	39.8	2205.3	451.1
5	143.0	29.7	346.0	70.9	2001.8	415.3
4	138.6	28.1	489.0	100.6	1940.9	393.9
3	133.2	26.9	627.7	128.7	1864.2	376.2
2	161.4	28.7	760.8	155.6	2904.7	516.3
Total	922.2	184.3	922.2	184.3	10916.9	2152.9

Note: Total Base Shear includes load from Windward and Leeward pressures

Final Report

APPENDIX D: SEISMIC LOAD CALCULATIONS

Table 26: Seismic Design Values

Seismic Design Values, ASCE 7-05			
Response Modification Coefficient	R= 3	R= 3.5	Table 12.2-1
Coefficient	$C_U= 1.7$	$C_U= 1.7$	Table 12.8-1
Fundamental Period	T= 1.497	T= 1.497	Sec. 12.8.2
Seismic Response Coefficient	$C_S= 0.016$	$C_S= 0.014$	Eq. 12.8-3
Building Height (above grade)	h= 74.5	h= 74.5	

Table 27: Seismic Design Values continued

Seismic Design Values, ASCE 7-05		
Occupancy	II	Table 1-1
Importance Factor	I= 1	Table 11.5-1
Site Class	D	Table 20.3-1
Spectral Response Acceleration, short	$S_S= 0.12$	Figure 22-1
Spectral Response Acceleration, 1 sec	$S_1= 0.046$	Figure 22-2
Site Coefficient F_a	$F_a= 1.6$	Table 11.4-1
Site Coefficient F_V	$F_V= 2.4$	Table 11.4-2
MCE Spectral Response Acceleration, short	$S_{MS}= 0.192$	Eq. 11.4-1
MCE Spectral Response Acceleration, 1 sec	$S_{M1}= 0.1104$	Eq. 11.4-2
Design Spectral Acceleration, short	$S_{DS}= 0.128$	Eq. 11.4-3
Design Spectral Acceleration, 1 sec	$S_{D1}= 0.0736$	Eq. 11.4-4
Seismic Design Category	B	Table 11.6-1

Table 28: F_V Values

F_V Values (Table 11.4-2 ASCE 7-05)					
	$S_1 \leq 0.1$	$S_1 = 0.3$	$S_1 = 0.3$	$S_1 = 0.4$	$S_1 \geq 0.5$
D	2.4	2	1.8	1.6	1.5

Table 29: F_a Values

F_a Values (Table 11.4-1 ASCE 7-05)					
	$S_S \leq 0.25$	$S_S = 0.5$	$S_S = 0.75$	$S_S = 1.0$	$S_S \geq 1.25$
D	1.6	1.4	1.2	1.2	1

Final Report

SEISMIC CALCULATIONS CONTINUED:

The values for all the seismic coefficients were determined using ASCE 7-05 equations and tables. The building was first confirmed as Seismic design category B by using Table 11.6-2 of ASCE 7-05. Once the design category had been confirmed, the approximate period was calculated by using equation 12.8-7 and table 12.8-2. Since ASCE 7-05 section 11.6 requires where an S_1 value is less than 0.75 the Seismic Design Category can be determined solely on table 11.6-1 and 11.6-2 when $T_a > 0.8T_s$, the period used to calculate drift is less than T_s , equation 12.8-2 is used to find C_s , and rigid diaphragms are present.

Table 30: Seismic Response Value Comparison

Calculated Values		USGS Website Values
$S_S = 0.12$	(From Figure 22-1)	$S_S = 0.125$
$S_1 = 0.046$	(From Figure 22-2)	$S_1 = 0.048$
$S_{MS} = F_a * S_S = 0.192$		$S_{MS} = 0.2$
$S_{M1} = F_V * S_1 = 0.1104$		$S_{M1} = 0.116$
$S_{DS} = 2S_{MS}/3 = 0.128$	A (Table 11.6-1)	$S_{DS} = 0.133$
$S_{D1} = 2S_{M1}/3 = 0.0736$	B (Table 11.6-2)	$S_{D1} = 0.077$

$C_T = 0.016$ (From Table 12.8-2)

$X = 0.9$ (From Table 12.8-2)

$T_a = C_t h_n^x = 0.9411255$

$T_s = S_{D1}/S_{DS} = 0.575$

$0.8T_s = 0.46 < T_a$ therefore must use Table 11.6-1,2

$T_L = 12$ (From Fig. 22-15 p. 228 ASCE 7-05)

C_s values were calculated according to Section 12.8.1.1 equations 12.8-2, 12.8-3, and 12.8-4 and checked against the minimum requirement from EQ 12.8-5 of $C_s \geq 0.01$. Equation 12.8-3 is a maximum for this structure, and equation 12.8-4 does not apply since equation 12.8-3 does. The values were then compared based on R and what the professional calculated.

Final Report

$$\begin{array}{l}
 C_s = \text{MAX} \\
 \text{for } T > T_L
 \end{array}
 \left|
 \begin{array}{l}
 R=3 \\
 S_{DS}/(R/I) = 0.0427 \\
 S_{D1}/(T^*R/I) = 0.0153 \\
 S_{D1}T_L/(T^2R/I) = 0.3324 \\
 \geq 0.01
 \end{array}
 \right.$$

$$\begin{aligned}
 C_s &= 0.0153 \\
 T &= C_U * T_a = 1.5999134
 \end{aligned}$$

$$\begin{aligned}
 k &= 1.550 \\
 W &= 106734.9 \\
 V &= C_s * W = 1636.69
 \end{aligned}$$

The floor weights used for the seismic calculations were calculated using a 10" NWC slab over the entire area, added to the column weights. Also, the superimposed loads were added and a bracing allowance to account for beams as part of the floor system.

Table 31: Beams on 4th floor with total beam weight

Beams:			
Shape	Unit Weight (lb/ft)	Beam Length (ft)	Total Weight
32x34	1095.56	0	0.0 kips
30x34	1027.08	0	0.0 kips
34x34	1164.03	48	55.9 kips
24x34	821.667	5443.9	4473.1 kips
Total Weight=	4528.9 kips		

Final Report

Table 32: Fourth Floor weight calculation

Floor # 4					
Approx. Area:		64231.7 ft ²		Floor to Floor Height: 14	
Slab:					
NWC		145 PCF			
Thickness=		10 inches			
unit weight=		120.8333 psf			
total weight=		7761 kips			
Columns:					
Shape	Quantity	Unit Weight (lb/ft)	Column Height (ft)	Total Weight	
24x24	102	580	14	828.2	kips
28x28	3	789.44444	14	33.2	kips
30x30	6	906.25	14	76.1	kips
32x32	0	1031.1111	14	0.0	kips
34x34	0	1164.0278	14	0.0	kips
36x36	0	1305	14	0.0	kips
48x48	0	2320	14	0.0	kips
Column Reinf =		22.35 Kips			
X-verse Reinf=		2.77 kips			
Total Weight=		962.6 kips			
Beam =		4528.9 kips			
Reinforcement=		156.177 kips			
Total Weight=		4685.1 kips			
Super Imposed:					
MEP=		5 psf			
Finishes=		3 psf			
Total Weight=		513.9 kips			
TOTAL FLOOR WEIGHT:			13922.9	or	216.8
			kips		psf

Final Report

The values in this portion of the report were calculated using the method described in the Seismic design portion of this report and the same method used in Technical Report One.

Table 33: Seismic Forces, Shears and Moments for As- Built with R=3

R=3

Floor	w_x (k)	h_x (ft)	h_x^k (ft)	$w_x h_x^k$	C_{vx}	Story Force F_x (k)	Story Shear V_x (k)	Moment at Floor (ft-k)
Roof	4240.5	74.5	639.41	2711449	0.359	167.42	0	12473.065
5	4713.6	60	462.27	2178985	0.288	134.55	167.42	8072.7394
4	4726.5	46	310.43	1467216	0.194	90.60	301.97	4167.4204
3	4724.0	32	180.20	851252	0.113	52.56	392.57	1681.9916
2	4653.4	18	76.08	354028	0.047	21.86	445.13	393.48265
1	5444.4						466.99	
Sum	28502.4	74.5	1668.39	7562930	1.000	466.99	466.99	26788.699

Table 34: Seismic Forces, Shears, and Moments for As-Built with R=3.5

R=3.5

Floor	w_x (k)	h_x (ft)	h_x^k (ft)	$w_x h_x^k$	C_{vx}	Story Force F_x (k)	Story Shear V_x (k)	Moment at Floor (ft-k)
Roof	4240.5	74.5	639.41	2711449	0.359	143.51	0	10691.199
5	4713.6	60	462.27	2178985	0.288	115.32	143.51	6919.4909
4	4726.5	46	310.43	1467216	0.194	77.65	258.83	3572.0746
3	4724.0	32	180.20	851252	0.113	45.05	336.48	1441.7071
2	4653.4	18	76.08	354028	0.047	18.74	381.54	337.27085
1	5444.4						400.28	
Sum	28502.4	74.5	1668.39	7562930	1.000	400.28	400.28	22961.742

Table 35: Seismic Forces, Shears, and Moments for Redesigned with R=3

Floor	w_x (k)	h_x (ft)	h_x^k (ft)	$w_x h_x^k$	C_{vx}	Story Force F_x (k)	Story Shear V_x (k)	Moment at Floor (ft-k)
Penthouse	6481.1	92.5	1115.41	7229044	0.179	293.33	0	27133.348
Roof	18245.1	74.5	797.56	14551503	0.361	590.46	293.33	43989.083
5	14162.0	60	570.24	8075727	0.200	327.69	883.79	19661.364
4	13922.9	46	377.75	5259370	0.130	213.41	1211.48	9816.8534
3	16960.3	32	215.24	3650482	0.091	148.13	1424.89	4740.0283
2	17785.3	18	88.23	1569200	0.039	63.67	1573.02	1146.1239
1	19178.2						1636.69	
Sum	106734.9	92.5	3164.42	40335326	1.000	1636.69	1636.69	106486.8

Final Report

APPENDIX E: MEMBER DESIGNS AND CHECKS

Interior 45' span beam Design

GIRDER DESIGN - INTERIOR - FLOOR

LOADING: DEAD: 125 PSF + 8 PSF + GIRDER WT
 LIVE: 50 PSF + 20 PSF

* NO LIVE LOAD REDUCTION TO BE CONSERVATIVE
 SINCE TENANT FIT-OUT DWGS UNAVAILABLE

$W_u = 1.2(125+8) + 1.6(50+20) = 272 \text{ PSF}$

$W_u = 272 \text{ PSF}$

MAXIMUM MOMENT DETERMINATION

$M_{MAX @ ENDS} = \frac{w_l^2}{12} = \frac{(0.272 \text{ KSF})(24)(45)^2}{12} = 110.6 \text{ k-ft}$

$M_{MAX @ MID} = \frac{w_l^2}{24} = \frac{(0.272 \text{ KSF})(24)(45)^2}{24} = 550.8 \text{ k-ft}$

GIRDER SIZE

$b d^2 = 20 M_u$
 $24(d)^2 = 20(1102)$
 $d = 30.3''$ TRY #8'S

$h = d + 1.5 + d_b/2 = 30.3 + 1.5 + 1/2 = 32.3$
 $h = 34''$ $d = h - 1.5 - 3d_b/2 = 34 - 1.5 - 3/2 = 31$

$A_s = \frac{M_u}{\frac{f_y}{4} a} = \frac{1102}{\frac{4(31)}{4(31)}} = 8.89 \text{ in}^2$

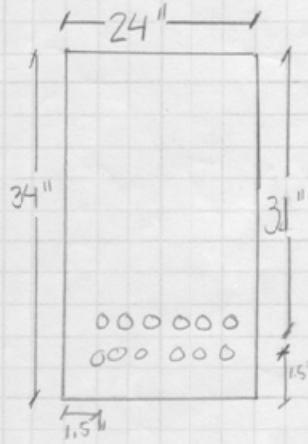
- TRY 12 # 8'S IN 2 ROWS, $A_s = 9.48 \text{ in}^2$
- ASSUME $f_s > f_y$

$a = \frac{A_s f_y}{0.85 f_c b} = \frac{(9.48)(60)}{0.85(4)(24)} = 6.97''$

$c = a/\beta_1 = 6.97/0.85 = 8.2''$

- CHECK $f_s > f_y$
 $f_s = \epsilon_u/c(d-c) = 0.003/8.2(31-8.2) = 0.0083 > 0.005 \therefore \text{OK } \phi = 0.9$

$\phi M_n = \phi A_s f_y (d - a/2) = 0.9(9.48)(60)(31 - 6.97/2) = 14085.5 \text{ k-in}$
 $\phi M_n = 1173.8 \text{ k-ft} > M_u = 1102 \text{ k-ft} \therefore \text{OK}$



Final Report

MEMBER DESIGN CONTINUED:

• CHECK SHEAR

$$V_n = V_c + V_s \quad \phi V_n \geq V_u$$

• SHEAR STRENGTH OF CONC. BM w/o STIRREPS

$$V_c = 2 \lambda \sqrt{f'_c} b_w d$$

$$= 2(1) \sqrt{4000} (24)(31) = 94.1^k$$

$$\phi V_n = 0.5 \phi V_c = 0.5(0.75)(94.1) = 35.3^k$$

• DETERMINE SHEAR STRENGTH REQUIRED BY REINFORCING

$$V_u @ d = 170 - 7.54(31/12) = 150.5$$

• DETERMINE MAXIMUM SPACING OF SHEAR REINF.

IF $V_s \leq 4 \sqrt{f'_c} b_w d = 188.2^k$ THEN $S_{MAX} = \min \left\{ \begin{array}{l} d/2 = 31/2 = 15.5'' \\ 24'' \end{array} \right.$

$$V_s = 106.6^k < 188.2$$

ELSE $S_{MAX} = \min \left\{ \begin{array}{l} d/4 = \\ 12'' \end{array} \right.$

$S = 15''$

Final Report

MEMBER DESIGN CONTINUED:

• DETERMINE MINIMUM SHEAR REINF.

$$A_{U\text{MIN}} = \text{MAX} \begin{cases} 0.75 \sqrt{f'_{cs}} b_w s / f_{yt} = 0.75 \sqrt{4000} (24)(15) / 60000 = 0.285 \text{ IN}^2 \\ 50 b_w s / f_{yt} = 50(24)(15) / 60000 = 0.3 \text{ IN}^2 \end{cases}$$

$$A_{U\text{MIN}} = 0.3 \text{ IN}^2$$

USE #3 STIRRUPS @ 15" AS MINIMUM SHEAR REINF.
 (3 LEGS = 3(0.11 IN²) = 0.33 IN² > 0.3 IN² ✓ OK

• DESIGN SHEAR REINF.

$$V_s = A_v f_{yt} d / s$$

$$s = \frac{A_v f_{yt} d}{V_s} = \frac{0.33(60)(31)}{100.6} = 5.76''$$

USE (3) #3 @ 5" AT MEMBER ENDS, STARTING 2" FROM FACE OF SUPPORT

• FIND WHERE (3) #3 @ 12" WORKS

$$\phi V_n = \phi V_c + \phi V_s = 0.75 \left(94.1 + \frac{0.33(60)(31)}{12} \right) = 108.9375^k$$

DISTANCE WHERE $V_u = 108.9375^k$

$$L_v = \frac{(170 - 108.9)(12 \text{ ft})}{7.54 \text{ k/ft}} = 97.25'' = 8' - 1\frac{1}{4}''$$

$\leftarrow 97.3'' \quad | \quad 62.7'' \quad | \quad 110'' \quad | \quad 62.7'' \quad | \quad 97.3'' \rightarrow$
 $\leftarrow 20 \#5'' \quad | \quad 5 \#12'' \quad | \quad \text{NO STIRR. REQUIRED} \quad | \quad 5 \#12'' \quad | \quad 20 \#5'' \rightarrow$

Final Report

MEMBER DESIGN CONTINUED:

Interior slab thickness design

INTERIOR DESIGN

LOADING : 50 OFFICE LOADS-LIVE
20 PARTITION LOAD-LIVE
8 SUPERIMPOSED DEAD (FORMER, ETC)
+ ? CONC SLAB

$$W_u = 1.2(8 \text{ PSF}) + 1.6(70) = 121.6 \text{ PSF}$$

MATERIALS : $f'_c = 4000 \text{ PSI}$
 $f_y = 60 \text{ KSI}$

MINIMUM SLAB THICKNESS :

- ASSUME COLUMNS ARE 24" X 24"

$$l_n = 24' - 2' = 22'$$

- FROM ACI 318-08, TABLE 9.5 $h > l_n / 28$
 $h > (22 \times 12) / 28$
 $h > 9.43" \rightarrow \boxed{h = 10"}$

SLAB CONTRIBUTION TO DEAD LOAD

$$\text{SLAB WEIGHT} = 150 \text{ PCF} \times \frac{10"}{12"/\text{ft}} = 125 \text{ PSF}$$
$$W_{\text{SLAB}} = 1.2(125 \text{ PSF}) = 150 \text{ PSF}$$

TOTAL LOAD :

$$W_u = 121.6 \text{ PSF} + 150 \text{ PSF} = 271.6 \text{ PSF}$$
$$\boxed{W_u = 272 \text{ PSF}}$$

MOMENT VALUES USING ACI COEFFICIENTS

- AT INTERIOR SUPPORTS: $-M = \left(\frac{1}{10}\right) w_u l_n^2 = \left(\frac{1}{10}\right) (272) (22)^2 = 13.165 \text{ k-ft}$
- AT MIDSPAN: $+M = \left(\frac{1}{16}\right) w_u l_n^2 = \left(\frac{1}{16}\right) (272) (22)^2 = 8.228 \text{ k-ft}$
- UNFACTORED : $M_u = \frac{w l^2}{8} = \frac{(70 + 8 + 125)(22)^2}{8} = 12.282 \text{ k-ft}$

Final Report

MEMBER DESIGN CONTINUED:

REQUIRED REINFORCEMENT

- $\rho_{MAX} = 0.85\beta (f_c/f_y) \left[\frac{\epsilon_s}{\epsilon_s + \epsilon_t} \right]$
- $\rho_{MAX} = 0.85(0.85) \left(\frac{4}{100} \right) \left[\frac{0.003}{0.003 + 0.004} \right] = 0.0206$
- EFFECTIVE DEPTH:
 $bd^2 = 20M_u$
 $(12")(d^2) = 20(13.165 \text{ K-ft})$
 $d = 4.68"$
- AREA OF STEEL REQUIRED PER FOOT IN TOP OF SLAB:
 $A_s = \frac{M_u}{4d}$
 $A_s = \frac{13.165}{4 \times 4.68} = 0.703 \text{ in}^2$
 $\text{USE \# 8 @ 12" } (A_s = 0.79 \text{ in}^2)$
- AREA OF STEEL REQUIRED PER FOOT @ MIDSPAN:
 $A_s = \frac{M_u}{4d}$
 $A_s = \frac{8.228}{4 \times 4.68} = 0.4395 \text{ in}^2$
 $\text{USE \# 8 @ 12" } (A_s = 0.79 \text{ in}^2) \text{ (FOR EASE OF CONSTRUCTION)}$
- MINIMUM STEEL FOR SHRINKAGE + TEMPERATURE
 $A_{sMIN} = 0.0018(12")(10") = 0.216 \text{ in}^2$
 $A_{sMIN} = 0.216 \text{ in}^2 < A_s = 0.31 \text{ in}^2 \therefore \text{OK}$
 $\text{USE \# 5 @ 12" O.C.}$

Final Report

MEMBER DESIGN CONTINUED:

CHECK SHEAR

- SHEAR IN END MEMBERS @ FIRST INTERIOR SUPPORT
$$V_u = \frac{1.15 w_u l_n}{2} = \frac{1.15(0.272)(22)}{2} = 3.44 \text{ K}$$
- SHEAR AT OTHER SUPPORTS
$$V_u = \frac{w_u l_n}{2} = \frac{(0.272)(22)}{2} = 2.99 \text{ K}$$
- ALLOWABLE SHEAR
$$\phi V_n = 0.75(2)\sqrt{f'_c} \cdot bd$$
$$\phi V_n = 0.75(2)\sqrt{4000}(12)(4.68)$$
$$\phi V_n = 4.97 \text{ K}$$

$V_u < \phi V_n \therefore \text{OK}$

DEFLECTION CHECK (TABLE 9.5 CONFIRMATION)

$$\Delta = \frac{5 w_u l^4}{384 EI}$$
$$I = \frac{(24' \times 12''/12)(12'')^3}{12} = 41472 \text{ IN}^4$$
$$E = 57000\sqrt{4000} = 3605 \text{ KSI}$$
$$\Delta = \frac{5(0.272 \text{ KSF})(45')(24'')^4 (1728)}{384(3605 \text{ KSI})(41472 \text{ IN}^4)} = 0.611''$$
$$\Delta_{\text{MAX}} = \frac{l}{240} = \frac{24 \times 12}{240} = 1.2''$$

$\Delta_{\text{MAX}} > \Delta \therefore \text{OK}$

Final Report

MEMBER DESIGN CONTINUED: Third Floor Green Roof Slab Design

LOADING: 50 PSF DEAD
100 PSF LIVE
+ SELF

$$W_u = 1.2(50) + 1.6(100) = 220 \text{ PSF}$$

MATERIALS: $f'_c = 4000 \text{ PSI}$
 $f_y = 60 \text{ KSI}$

MINIMUM SLAB THICKNESS

- ASSUME COLUMNS ARE 24" x 24"

$$l_n = 24' - 2' = 22'$$

- FROM ACI 318-08, TABLE 9.5 $h \geq l_n / 28$
 $h \geq (22 \times 12) / 28$
 $h \geq 9.43" \rightarrow h = 10"$

SLAB CONTRIBUTION TO DEADLOAD

$$\text{SLAB WT} = 150 \text{ PCF} \times \frac{10"}{12 \text{ IN/FT}} = 125 \text{ PSF}$$
$$W_{\text{SLAB}} = 1.2(125) = 150 \text{ PSF}$$

TOTAL LOAD:

$$W_u = 220 \text{ PSF} + 150 \text{ PSF} = 370 \text{ PSF}$$

$W_u = 370 \text{ PSF}$

MOMENT VALUES USING ACI COEFFICIENTS

- AT INTERIOR SUPPORTS: $-M = \left(\frac{1}{10}\right) W_u l_n^2 = \frac{1}{10} (370)(22)^2 = 17.91 \text{ K-ft}$
- AT MIDSPAN: $+M = \frac{1}{16} W_u l_n^2 = \frac{1}{16} (370)(22)^2 = 11.19 \text{ K-ft}$
- UNFACTORED: $M_u = \frac{w l^2}{8} = \frac{(50 + 100 + 125)(22)^2}{8} = 16.64 \text{ K-ft}$

Final Report

MEMBER DESIGN CONTINUED:

REQUIRED REINFORCEMENT

- $\rho_{MAX} = 0.85\beta (f'_c/f_y) \left[\frac{\epsilon_s}{\epsilon_{STEEL}} \right]$
 $\rho_{MAX} = 0.85(0.85)(4/60) \left[\frac{0.003}{0.003+0.004} \right] = 0.0206$
- EFFECTIVE DEPTH:
 $bd^2 = 20M_u$
 $(12") \times d^2 = 20(16.64 \text{ k-ft})$
 $d = 5.27"$
- AREA OF STEEL REQUIRED PER FOOT IN TOP OF SLAB:
 $A_s = \frac{M_u}{4d} = \frac{16.64}{4 \times 5.27} = 0.789 \text{ IN}^2$
 $\boxed{\text{USE \# 8 @ 12"} (A_s = 0.79 \text{ IN}^2)}$
- AREA OF STEEL REQUIRED PER FOOT @ MIDSPAN:
 $A_s = \frac{M_u}{4d} = \frac{11.19}{4 \times 5.27} = 0.531 \text{ IN}^2$
 $\boxed{\text{USE \# 8 @ 12"} (A_s = 0.79 \text{ IN}^2)}$
- MINIMUM STEEL FOR SHRINKAGE + TEMPERATURE:
 $A_{sMIN} = 0.0018(12") \times (10") = 0.216 \text{ IN}^2$
 $A_{sMIN} = 0.216 \text{ IN}^2 < A_s = 0.31 \text{ IN}^2 \therefore \text{OK}$
 $\boxed{\text{USE \# 5 @ 12" O.C.}}$

Final Report

MEMBER DESIGN CONTINUED:

• CHECK SHEAR

- SHEAR IN END MEMBERS @ FIRST INTERIOR SUPPORT

$$V_u = \frac{1.15 w_u l_n}{2} = \frac{1.15(0.37)(22)}{2} = 4.68 \text{ k}$$

- SHEAR AT OTHER SUPPORTS

$$V_u = \frac{w_u l_n}{2} = \frac{(0.37)(22)}{2} = 4.07 \text{ k}$$

- ALLOWABLE SHEAR

$$\phi V_n = 0.75(2) \sqrt{f'_c} b d$$

$$\phi V_n = 0.75(2) \sqrt{4000} (12)(5.27)$$

$$\phi V_n = 6 \text{ k}$$

$$\boxed{\phi V_n = 6 \text{ k} > V_u = 4.68 \text{ k} \therefore \text{OK}}$$

Final Report

MEMBER DESIGN CONTINUED: TOP FLOOR GREEN ROOF SLAB DESIGN

LOADING: 8 PSF DEAD
100 PSF LIVE
+SELF

$$W_u = 1.2(8) + 1.6(100) = 169.6 \text{ PSF}$$

MATERIALS: $f'_c = 4000 \text{ PSI}$
 $f_y = 60 \text{ KSI}$

MINIMUM SLAB THICKNESS

- ASSUME 24" X 24" COLUMNS
 $l_n = 24' - 2' = 22'$
- FROM ACI 318-08, TABLE 9.5 $h \geq l_n / 28$
 $h \geq (22 \times 12) / 28$
 $h \geq 9.43'' \rightarrow h = 10''$

SLAB CONTRIBUTION TO DEADLOAD
SLAB WE = $150 \text{ PCF} \times \frac{10''}{12 \text{ in/ft}} = 125 \text{ PSF}$

$$W_{\text{SLAB}} = 1.2(125) = 150 \text{ PSF}$$

TOTAL LOAD:

$$W_u = 170 \text{ PSF} + 150 \text{ PSF} = 320 \text{ PSF}$$

$$W_u = 320 \text{ PSF}$$

MOMENT VALUES USING ACI COEFFICIENTS:

- AT INTERIOR SUPPORTS: $-M = \left(\frac{1}{10}\right) W_u l_n^2 = \frac{1}{10} (0.32)(22)^2 = 15.49 \text{ k-ft}$
- AT MIDSPAN: $+M = \frac{1}{16} W_u l_n^2 = \frac{1}{16} (0.32)(22)^2 = 9.68 \text{ k-ft}$
- UNFACTORED: $M_u = \frac{w l^2}{8} = \frac{(100+8+125)(22)^2}{8} = 14.1 \text{ k-ft}$

Final Report

MEMBER DESIGN CONTINUED:

REQUIRED REINFORCEMENT

$\rho_{MAX} = 0.85(0.85)(4/60) \left[\frac{0.03}{0.03+0.07} \right] = 0.0200$

• EFFECTIVE DEPTH:

$$bd^2 = 20Mu$$
$$12d^2 = 20(14.1) \rightarrow d = 4.85''$$

• AREA OF STEEL REQUIRED PER FOOT IN TOP OF SLAB:

$$A_s = \frac{Mu}{4d} = \frac{14.1}{4 \times 4.85} = 0.727 \text{ IN}^2$$

USE #8 @ 12" ($A_s = 0.79 \text{ IN}^2$)

• AREA OF STEEL REQUIRED PER FOOT @ MIDSPAN:

$$A_s = \frac{Mu}{4d} = \frac{9.68}{4 \times 4.85} = 0.50 \text{ IN}^2$$

USE #8 @ 12" ($A_s = 0.79 \text{ IN}^2$)

• MINIMUM STEEL REQ'D FOR SHRINKAGE + TEMPERATURE:

$$A_{sMIN} = 0.0018(12'')(10'') = 0.216 \text{ IN}^2$$
$$A_{sMIN} = 0.216 \text{ IN}^2 < A_s = 0.31 \text{ IN}^2 \therefore \text{OK}$$

USE #5 @ 12" O.C.

• CHECK SHEAR

• SHEAR IN END MEMBER @ FIRST INT. SUPPORT

$$V_u = \frac{1.15W_u l_n}{2} = \frac{1.15(0.32)(22)}{2} = 4.048 \text{ K}$$

• SHEAR @ OTHER SUPPORTS

$$V_u = \frac{W_u l_n}{2} = \frac{0.32(22)}{2} = 3.52 \text{ K}$$

• ALLOWABLE SHEAR

$$\phi V_n = 0.75(2) \sqrt{4000} (12)(4.85) = 5.52 \text{ K}$$

$\phi V_n = 5.52 \text{ K} > V_u = 4.05 \text{ K} \therefore \text{OK}$

Final Report

MEMBER CHECK CONTINUED: LATERAL BEAM GIRDER CHECK

GIRDER CHECK

LATERAL END MOMENT = 290 k [EQ LOAD]
LOADING: DEAD = 125 PSF + 8 PSF + 850 PLF
LIVE = 50 PSF + 20 PSF

$$W_u = 1.2(125+8)(12) + 1.2(850) + 1.6(50+20)(12)$$
$$W_u = 4279.2 \text{ PLF}$$

MAXIMUM MOMENT DETERMINATION

GRAVITY

$$M_{\text{MAX@ENDS}} = \frac{wL^2}{12} = \frac{(4.28 \text{ kLF})(30')^2}{12} = 462.2 \text{ k-ft}$$

$$M_{\text{MAX@MID}} = \frac{wL^2}{24} = \frac{(4.28 \text{ kLF})(30')^2}{24} = 231.1 \text{ k-ft}$$

GRAVITY + LATERAL [1.2D + 1.6L + 1.0E]

$$M_{\text{MAX@ENDS}} = 462.2 \text{ k-ft} + 290 \text{ k-ft} = 752.2 \text{ k-ft}$$

$$M_{\text{MAX@MID}} = 231.1 \text{ k-ft} + 290 \text{ k-ft} = 521.1 \text{ k-ft}$$

BM HAS (8) # 8'S IN 2 ROWS

$$\therefore d = 31''$$

$$A_s = 8(0.79 \text{ in}^2) = 6.32 \text{ in}^2$$

$$\phi M_n = \phi A_s f_y (d - a/2) \rightarrow a = \frac{A_s f_y}{0.85 f'_c b} = \frac{(6.32)(60)}{0.85(4)(24)} = 4.67''$$

$$\phi M_n = 0.9(6.32 \text{ in}^2)(60 \text{ ksi})(31'' - 4.67''/2)$$

$$\phi M_n = 9787 \text{ k-ft} = 815.6 \text{ k-ft} > M_u = 752.2 \text{ k-ft} \quad \checkmark \text{OK}$$

Final Report

MEMBER CHECK CONTINUED:

CHECK SHEAR

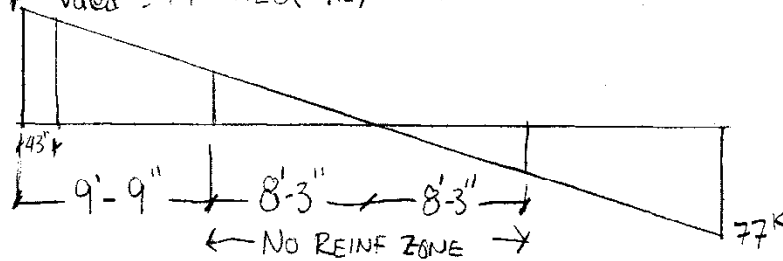
$$V_n = V_c + V_s \quad \phi V_n \geq V_u$$

SECTION OF CONC

$$V_c = 2 \lambda \sqrt{f_c} b_w d = 2 \sqrt{4000} (24)(31) = 94.1 \text{ K}$$

$$\phi V_n = 0.5 \phi V_c = 0.5(0.75)(94.1) = 35.29 \text{ K}$$

- DETERMINE SHEAR STRENGTH REQ'D BY REINFORCING
 $77 \text{ K} \quad V_{u@x} = 77 - 4.28(43/12) = 61.7 \text{ K}$



$$V_s = \frac{V_u}{\phi} - V_c = \frac{61.7}{0.75} - 94.1 = -11.88 \text{ K} \quad \therefore \text{MIN}$$

$$V_s \leq 8 \sqrt{f_c} b_w d = 8 \sqrt{4000} (24)(31) / 1000 = 376.4 \text{ K} \quad \checkmark \text{OK}$$

- DETERMINE MAX SPACING

If $V_s \leq 4 \sqrt{f_c} b_w d = 188.2 \quad \checkmark \text{OK}$ THEN $S_{MAX} = \begin{cases} 15.5" \\ 24" \end{cases}$

S = 15"

ELSE $S_{MAX} = \begin{cases} 12d \\ 24" \end{cases}$

Final Report

MEMBER CHECK CONTINUED:

DETERMINE MIN. SHEAR REINF.

$$A_{V \text{ MIN}} = \text{MAX} \left\{ \begin{array}{l} 0.75 \sqrt{f_c} b_w s / f_{yt} = 0.75 \sqrt{4000} (24)(15) / 60000 = 0.285 \text{ IN}^2 \\ 50 b_w s / f_{ye} = 50 (24)(15) / 60000 = 0.3 \text{ IN}^2 \end{array} \right.$$

$$A_{V \text{ MIN}} = 0.3 \text{ IN}^2$$

• BM HAS (3) #3 STIRRUPS, $A_s = 0.33 \text{ IN}^2 > A_{V \text{ MIN}} = 0.3 \text{ IN}^2 \therefore \text{OK}$

• CHECK SPACING

$$V_s = A_v f_{ye} \phi / s$$

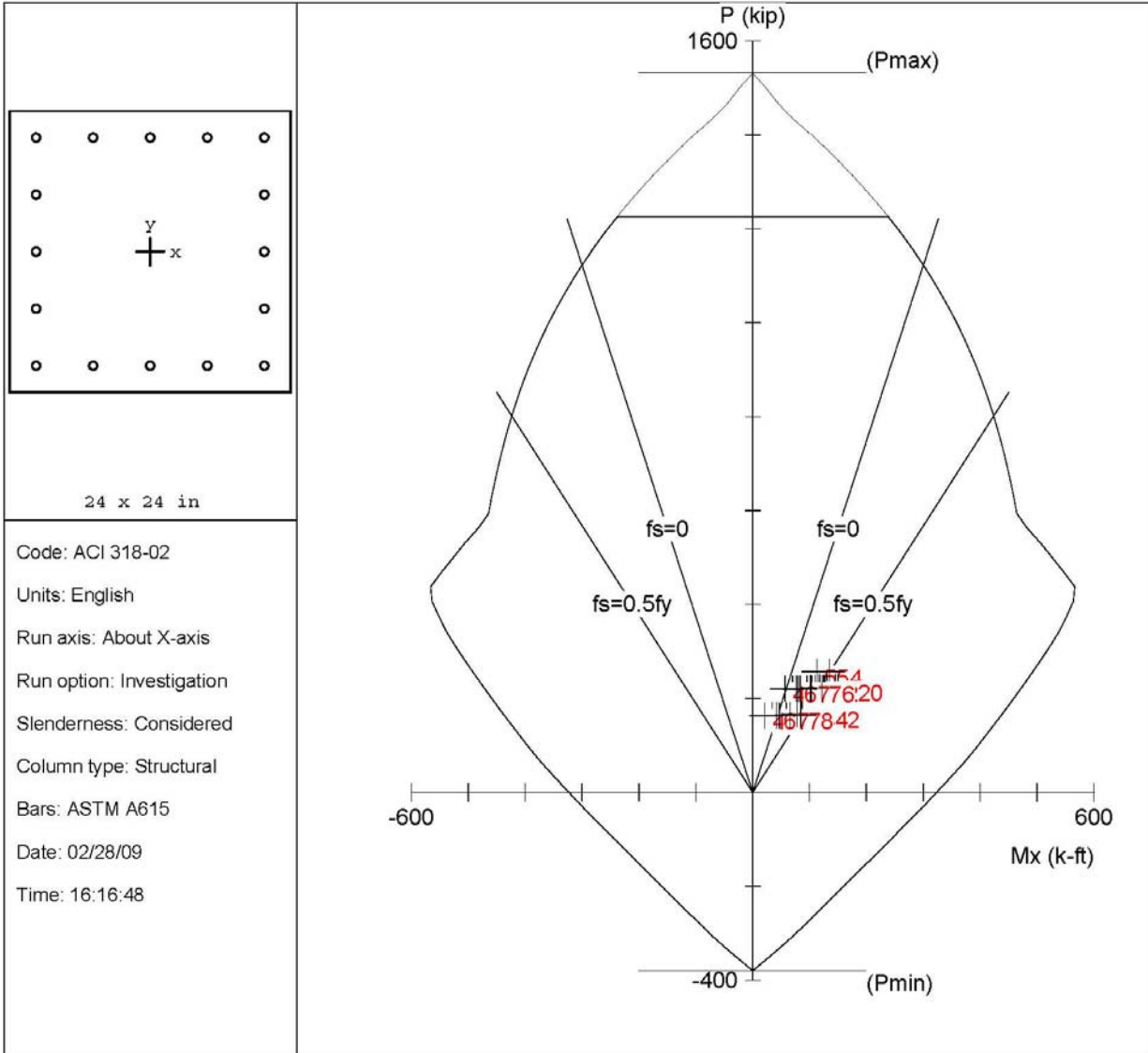
$$V_s = 11.9 \text{ " } \therefore \text{USE MAX SPACING}$$

$$S_{\text{MAX}} = 15 \text{ "}$$

$$\text{SPACING ON BM} = 9 \text{ " } \therefore \text{OK}$$

Final Report

MEMBER CHECK CONTINUED: COLUMN C-5 PENTHOUSE LEVEL



pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column5-C 6.col

Project:

Column:

$f_c = 4$ ksi

$E_c = 3605$ ksi

$f_c = 3.4$ ksi

$e_u = 0.003$ in/in

Beta1 = 0.85

Confinement: Tied

$k_x(\text{braced}) = 0.893474$, $k_x(\text{sway}) = \text{N/A}$

$f_y = 60$ ksi

$E_s = 29000$ ksi

$f_c = 3.4$ ksi

$\phi(a) = 0.8$, $\phi(b) = 0.9$, $\phi(c) = 0.65$

Engineer:

$A_g = 576$ in²

$A_s = 7.04$ in²

$X_o = 0.00$ in

$Y_o = 0.00$ in

Clear spacing = 4.13 in

16 #6 bars

Rho = 1.22%

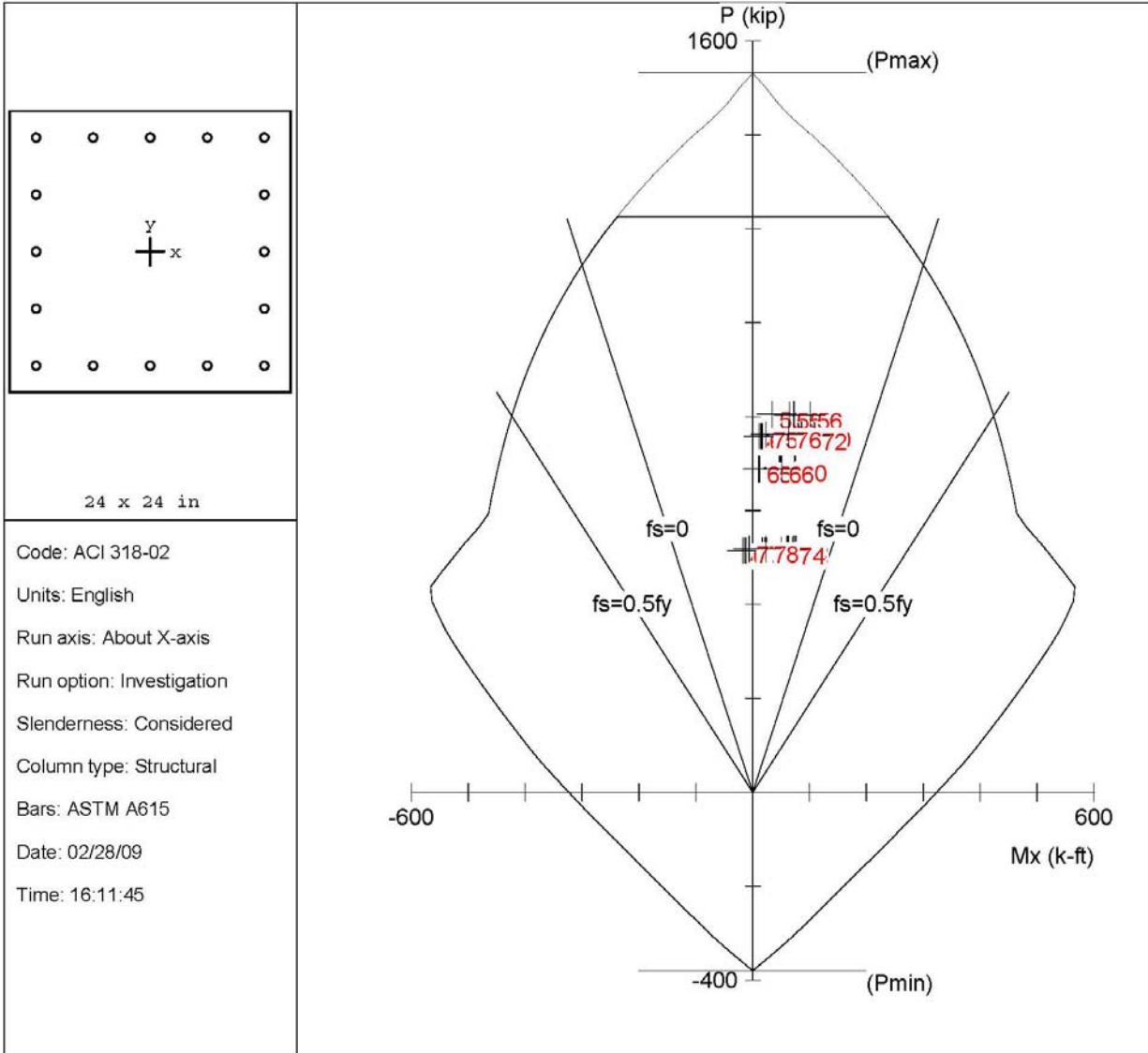
$I_x = 27648$ in⁴

$I_y = 27648$ in⁴

Clear cover = 1.88 in

Final Report

MEMBER CHECK CONTINUED: COLUMN C-5 FIFTH FLOOR



Code: ACI 318-02
 Units: English
 Run axis: About X-axis
 Run option: Investigation
 Slenderness: Considered
 Column type: Structural
 Bars: ASTM A615
 Date: 02/28/09
 Time: 16:11:45

pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column5-C 5.col

Project:

Column:

$f_c = 4$ ksi

$E_c = 3605$ ksi

$f_c = 3.4$ ksi

$e_u = 0.003$ in/in

Beta1 = 0.85

Confinement: Tied

$k_x(\text{braced}) = 0.963329$, $k_x(\text{sway}) = \text{N/A}$

$f_y = 60$ ksi

$E_s = 29000$ ksi

$f_c = 3.4$ ksi

$\phi(a) = 0.8$, $\phi(b) = 0.9$, $\phi(c) = 0.65$

Engineer:

$A_g = 576$ in²

$A_s = 7.04$ in²

$X_o = 0.00$ in

$Y_o = 0.00$ in

Clear spacing = 4.13 in

16 #6 bars

Rho = 1.22%

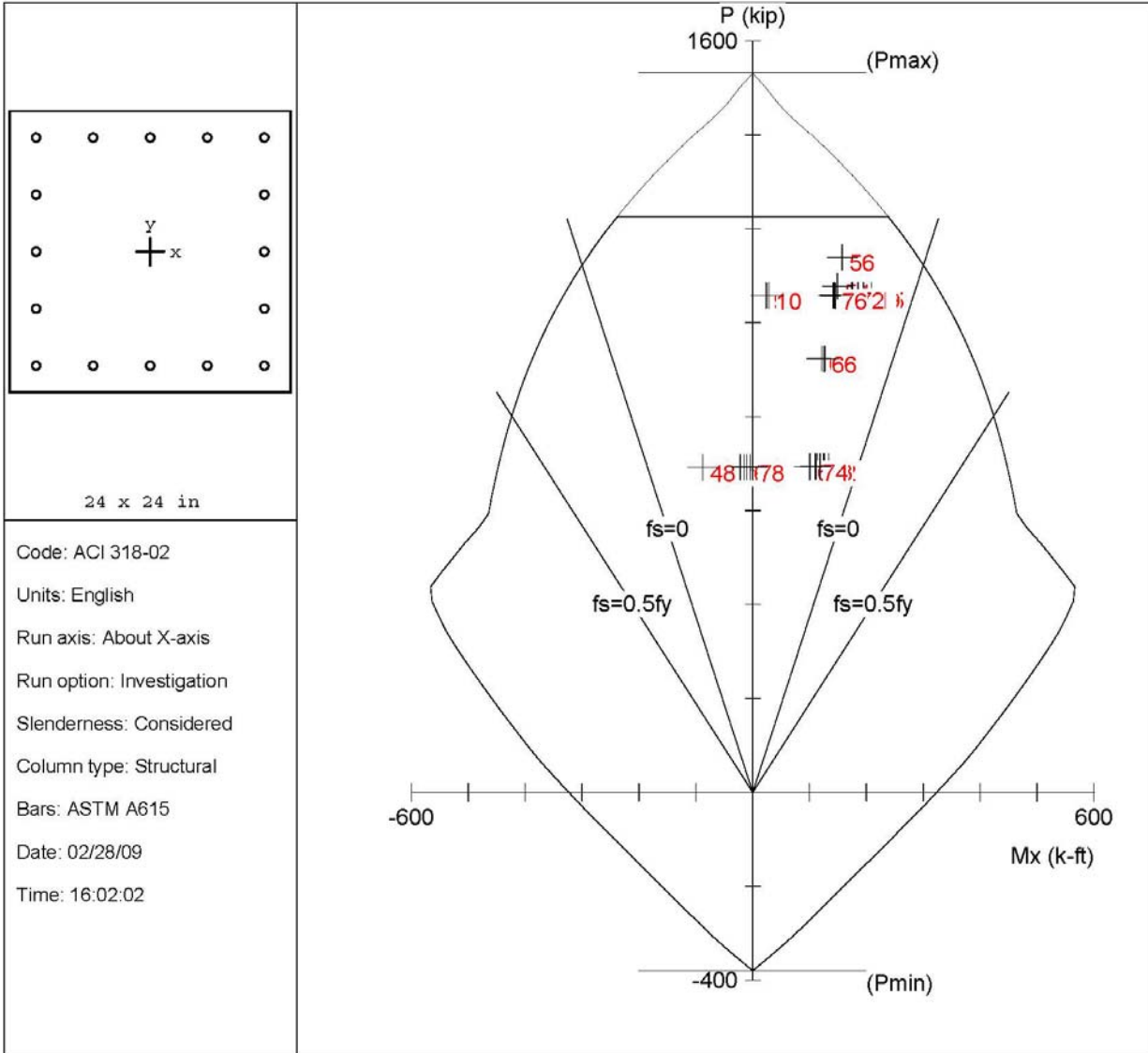
$I_x = 27648$ in⁴

$I_y = 27648$ in⁴

Clear cover = 1.88 in

Final Report

MEMBER CHECK CONTINUED: COLUMN C-5 FOURTH FLOOR



pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column5-C 4.col

Project:

Column:

$f_c = 4$ ksi

$E_c = 3605$ ksi

$f_c = 3.4$ ksi

$e_u = 0.003$ in/in

Beta1 = 0.85

Confinement: Tied

$k_x(\text{braced}) = 0.965049$, $k_x(\text{sway}) = \text{N/A}$

$f_y = 60$ ksi

$E_s = 29000$ ksi

$f_c = 3.4$ ksi

$\phi(a) = 0.8$, $\phi(b) = 0.9$, $\phi(c) = 0.65$

Engineer:

$A_g = 576$ in²

$A_s = 7.04$ in²

$X_o = 0.00$ in

$Y_o = 0.00$ in

Clear spacing = 4.13 in

16 #6 bars

Rho = 1.22%

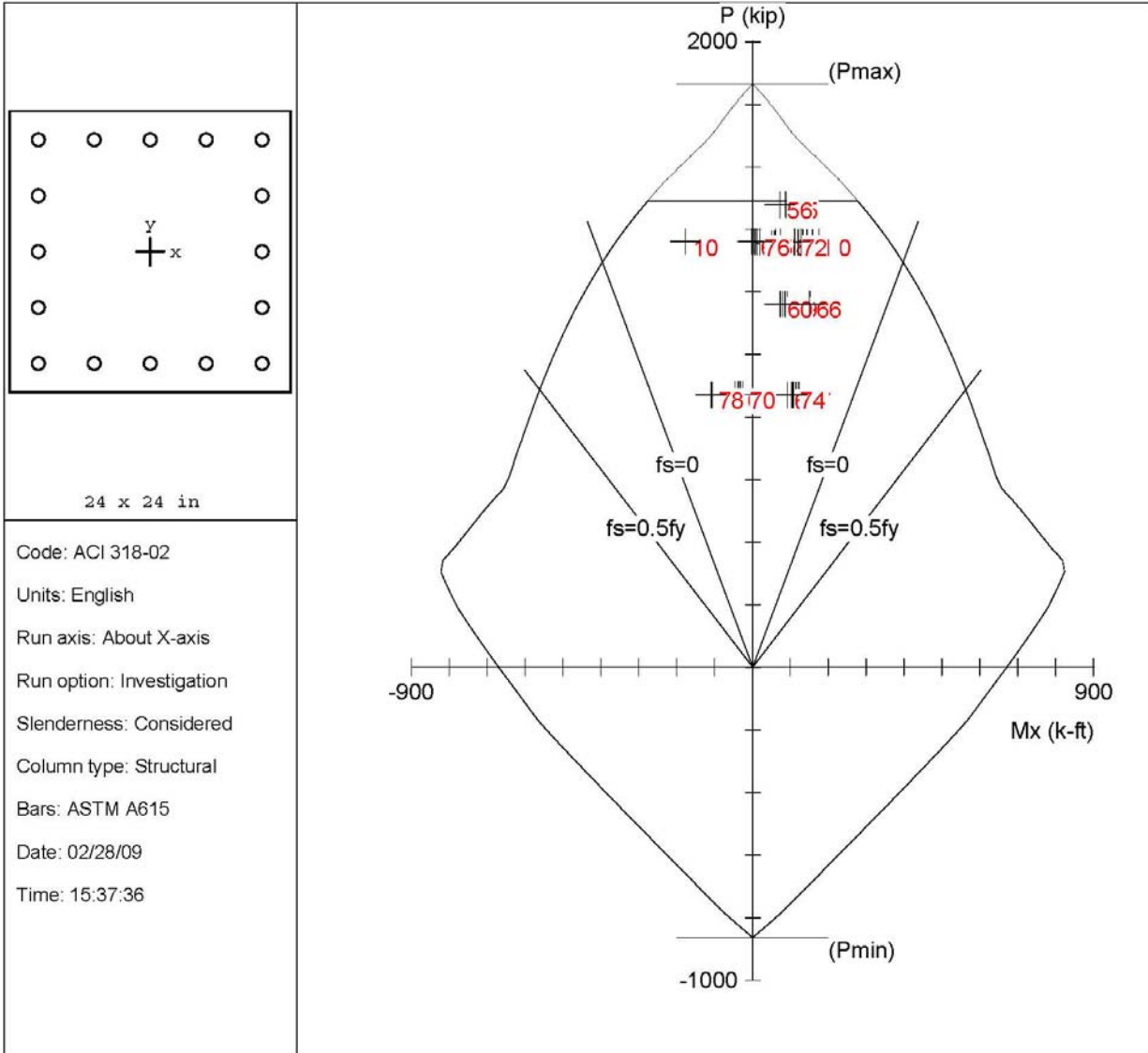
$I_x = 27648$ in⁴

$I_y = 27648$ in⁴

Clear cover = 1.88 in

Final Report

MEMBER CHECK CONTINUED: COLUMN C-5 THIRD FLOOR



pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column5-C 3.col

Project:

Column:

$f_c = 4$ ksi

$E_c = 3605$ ksi

$f_c = 3.4$ ksi

$e_u = 0.003$ in/in

Beta1 = 0.85

Confinement: Tied

$k_x(\text{braced}) = 0.965049$, $k_x(\text{sway}) = N/A$

$f_y = 60$ ksi

$E_s = 29000$ ksi

$f_c = 3.4$ ksi

$\phi(a) = 0.8$, $\phi(b) = 0.9$, $\phi(c) = 0.65$

Engineer:

$A_g = 576$ in²

$A_s = 16.00$ in²

$X_o = 0.00$ in

$Y_o = 0.00$ in

Clear spacing = 3.65 in

16 #9 bars

Rho = 2.78%

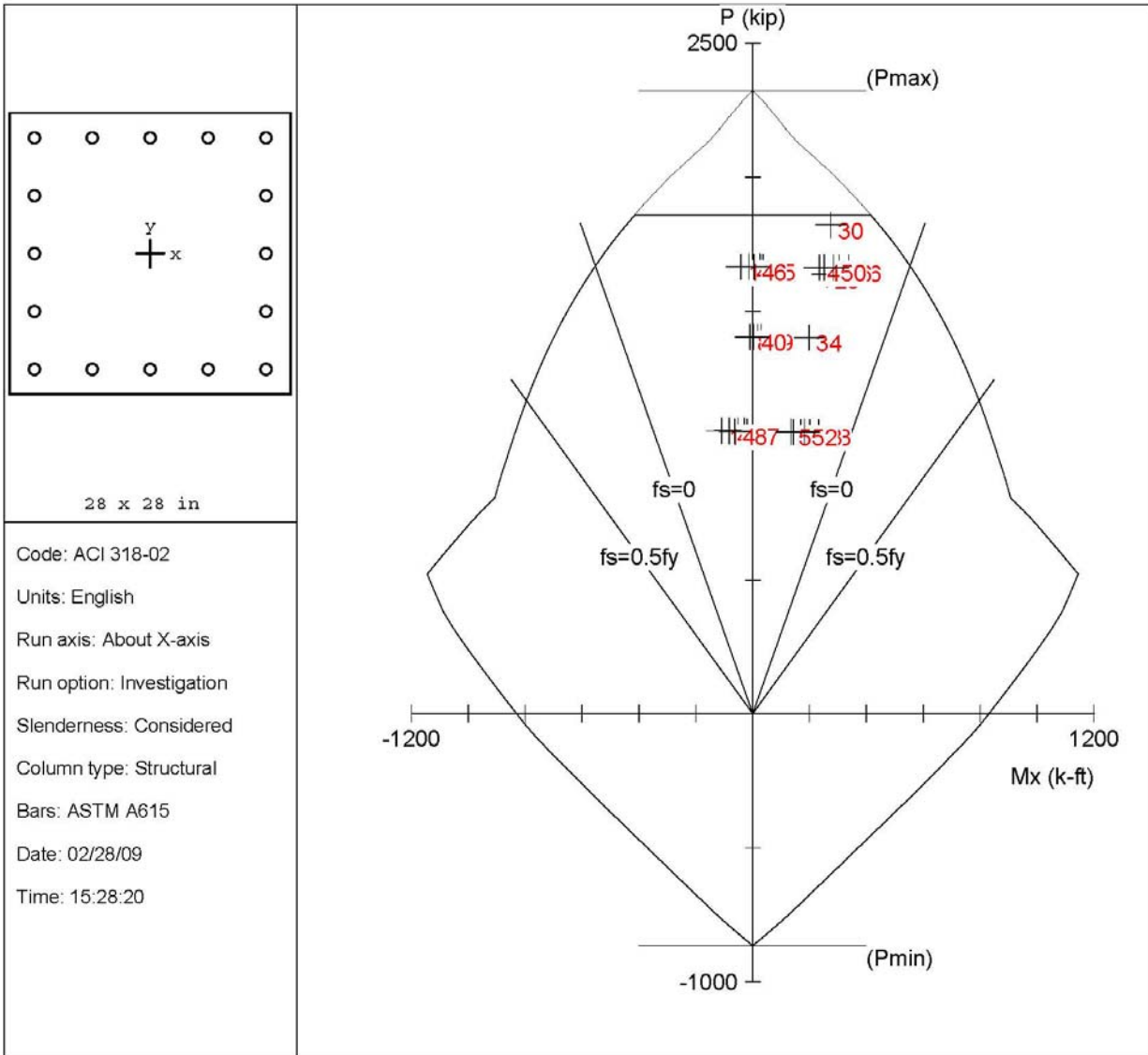
$I_x = 27648$ in⁴

$I_y = 27648$ in⁴

Clear cover = 1.88 in

Final Report

MEMBER CHECK CONTINUED: COLUMN C-5 SECOND FLOOR



28 x 28 in

Code: ACI 318-02
 Units: English
 Run axis: About X-axis
 Run option: Investigation
 Slenderness: Considered
 Column type: Structural
 Bars: ASTM A615
 Date: 02/28/09
 Time: 15:28:20

pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column5-C 2.col

Project:

Column:

$f_c = 4$ ksi

$E_c = 3605$ ksi

$f_c = 3.4$ ksi

$e_u = 0.003$ in/in

Beta1 = 0.85

Confinement: Tied

$k_x(\text{braced}) = 0.990837$, $k_x(\text{sway}) = \text{N/A}$

$f_y = 60$ ksi

$E_s = 29000$ ksi

$f_c = 3.4$ ksi

$\phi(a) = 0.8$, $\phi(b) = 0.9$, $\phi(c) = 0.65$

Engineer:

$A_g = 784$ in²

$A_s = 16.00$ in²

$X_o = 0.00$ in

$Y_o = 0.00$ in

Clear spacing = 4.65 in

16 #9 bars

Rho = 2.04%

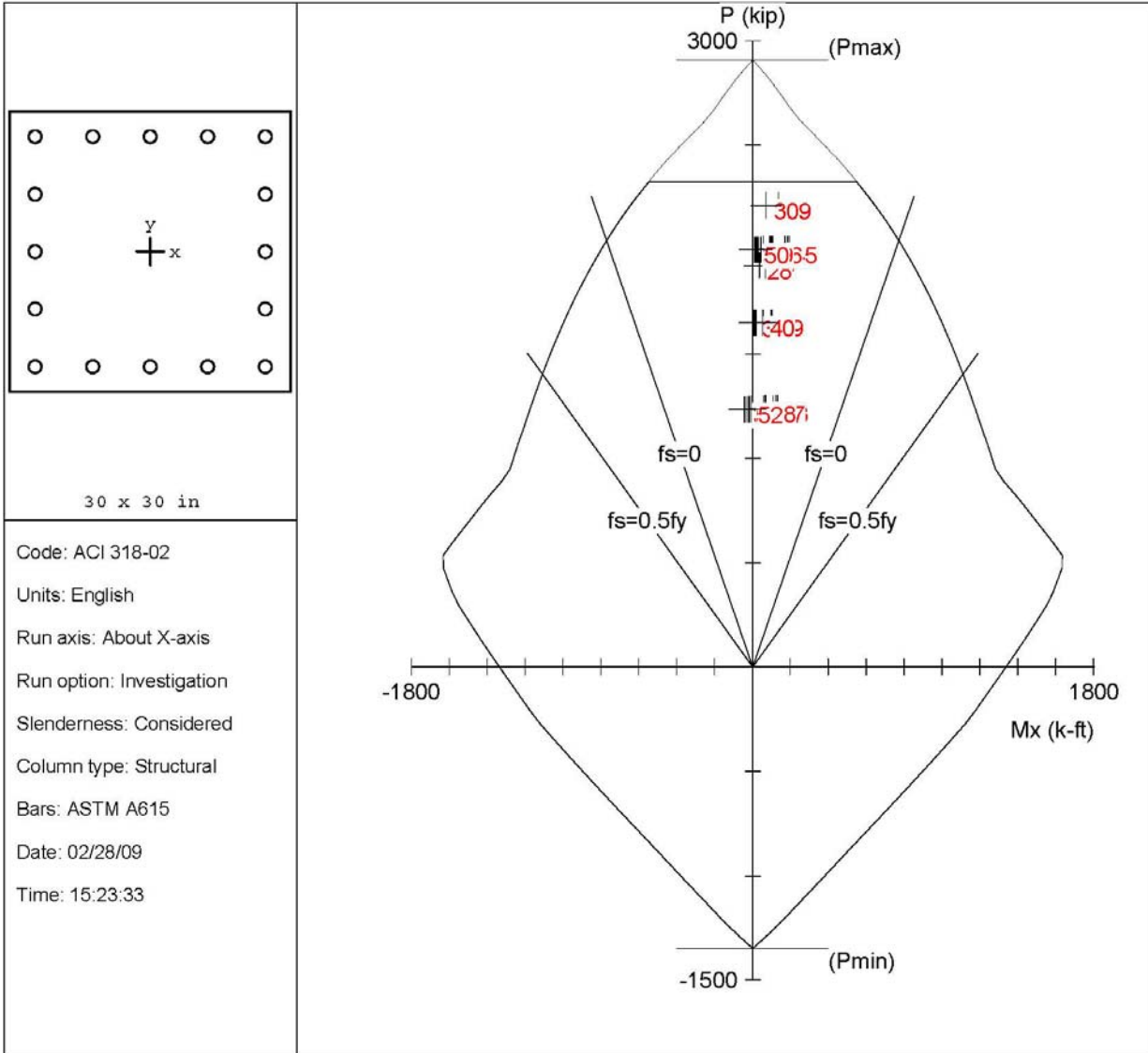
$I_x = 51221.3$ in⁴

$I_y = 51221.3$ in⁴

Clear cover = 1.88 in

Final Report

MEMBER CHECK CONTINUED: COLUMN C-5 FIRST FLOOR



Code: ACI 318-02
 Units: English
 Run axis: About X-axis
 Run option: Investigation
 Slenderness: Considered
 Column type: Structural
 Bars: ASTM A615
 Date: 02/28/09
 Time: 15:23:33

pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column5-C 1.col

Project:

Column:

$f_c = 4$ ksi

$E_c = 3605$ ksi

$f_c = 3.4$ ksi

$e_u = 0.003$ in/in

Beta1 = 0.85

Confinement: Tied

$k_x(\text{braced}) = 1, k_x(\text{sway}) = \text{N/A}$

$f_y = 60$ ksi

$E_s = 29000$ ksi

$f_c = 3.4$ ksi

$\phi(a) = 0.8, \phi(b) = 0.9, \phi(c) = 0.65$

Engineer:

$A_g = 900$ in²

$A_s = 24.96$ in²

$X_o = 0.00$ in

$Y_o = 0.00$ in

Clear spacing = 4.74 in

16 #11 bars

$Rho = 2.77\%$

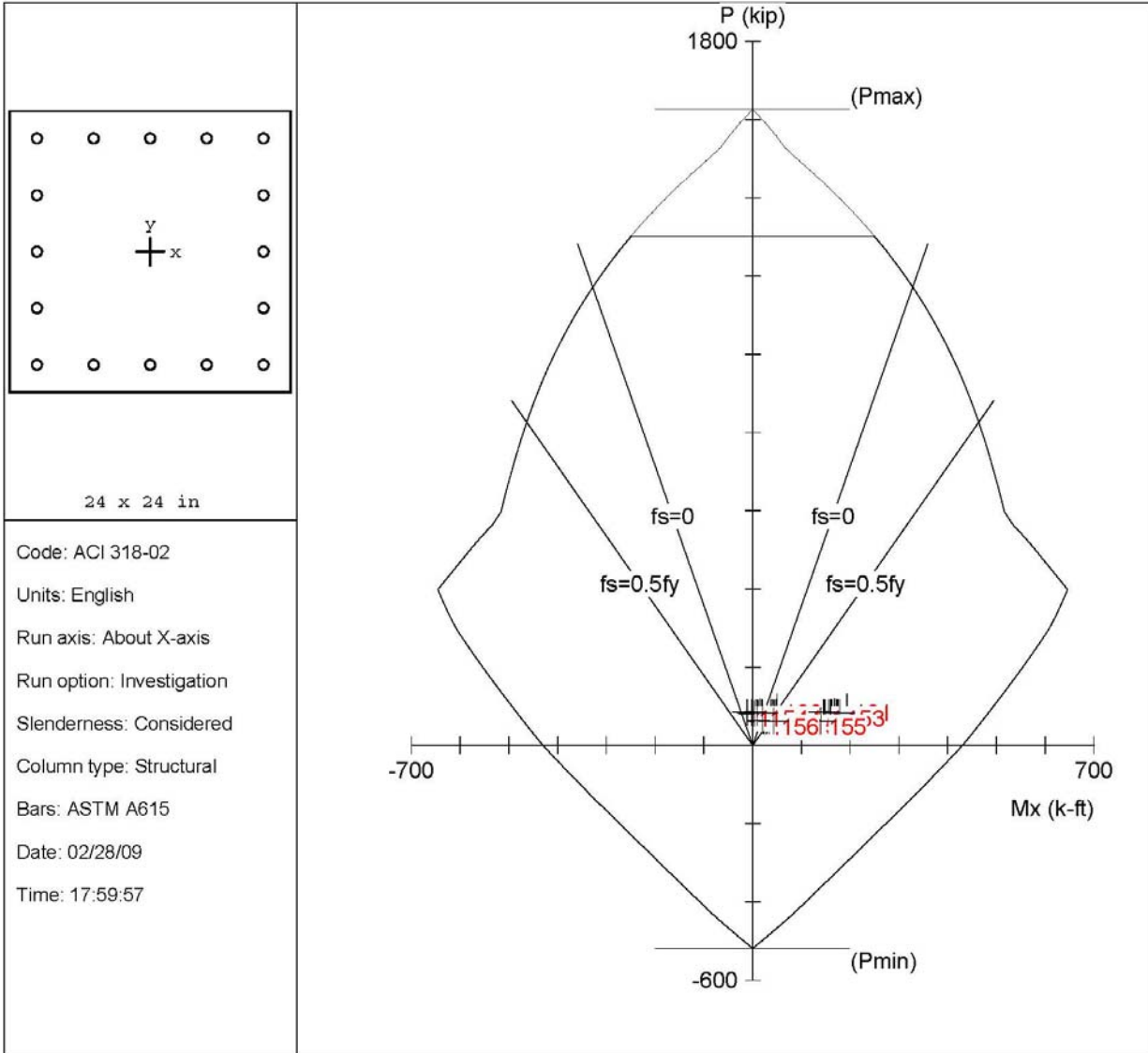
$I_x = 67500$ in⁴

$I_y = 67500$ in⁴

Clear cover = 2.00 in

Final Report

MEMBER CHECK CONTINUED: COLUMN D-7.9 PENTHOUSE FLOOR



pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column7.9-D 7.col

Project:

Column: 7.9-D 1

Engineer:

$f_c = 4$ ksi

$f_y = 60$ ksi

$A_g = 576$ in²

16 #7 bars

$E_c = 3605$ ksi

$E_s = 29000$ ksi

$A_s = 9.60$ in²

Rho = 1.67%

$f_c = 3.4$ ksi

$f_c = 3.4$ ksi

$X_o = 0.00$ in

$I_x = 27648$ in⁴

$e_u = 0.003$ in/in

$Y_o = 0.00$ in

$I_y = 27648$ in⁴

Beta1 = 0.85

Clear spacing = 3.97 in

Clear cover = 1.88 in

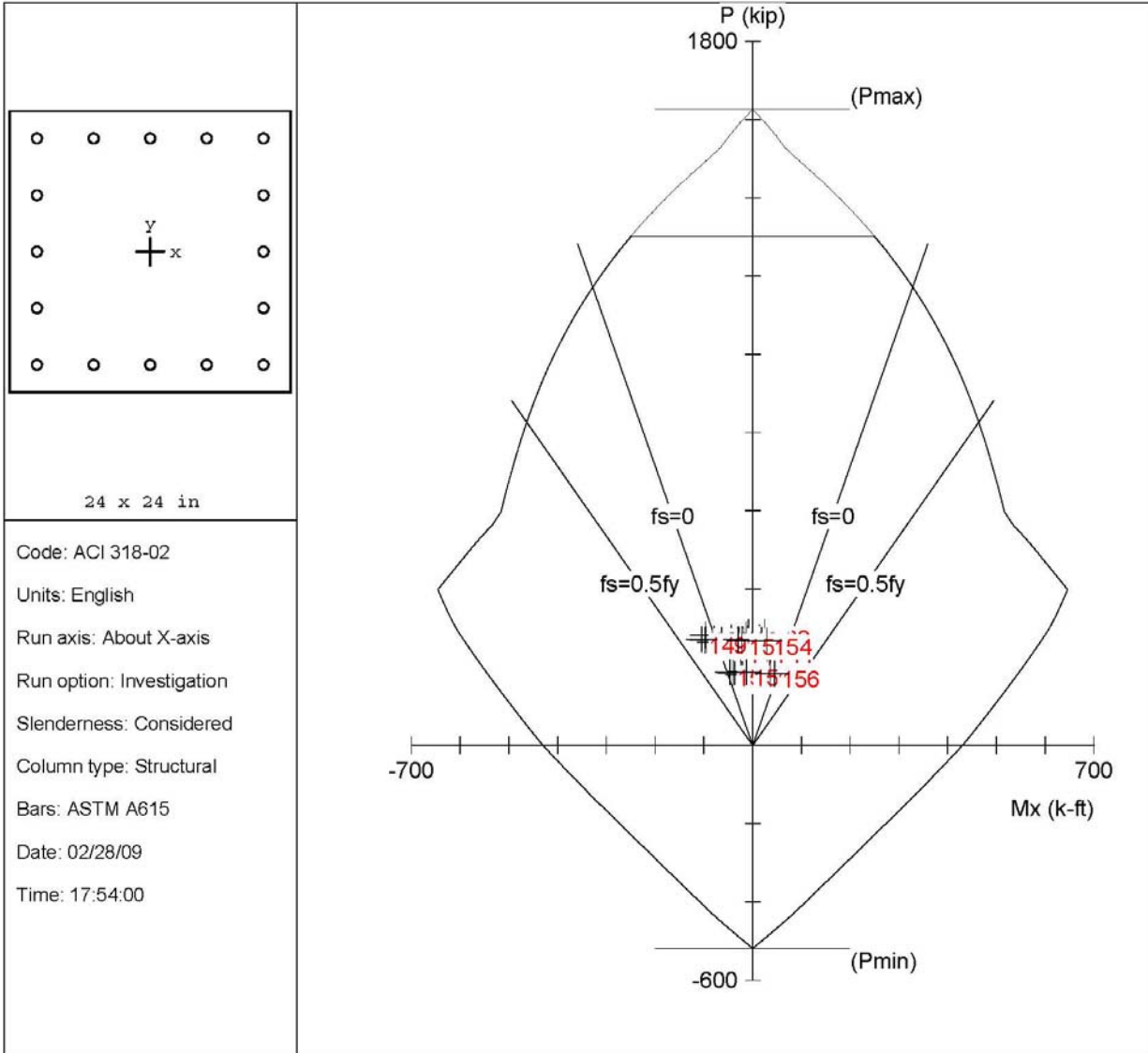
Confinement: Tied

$\phi(a) = 0.8, \phi(b) = 0.9, \phi(c) = 0.65$

$k_x(\text{braced}) = 0.893474, k_x(\text{sway}) = \text{N/A}$

Final Report

MEMBER CHECK CONTINUED: COLUMN D-7.9 FIFTH FLOOR



pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column7.9-D 6.col

Project:

Column: 7.9-D 1

Engineer:

$f_c = 4$ ksi

$f_y = 60$ ksi

$A_g = 576$ in²

16 #7 bars

$E_c = 3605$ ksi

$E_s = 29000$ ksi

$A_s = 9.60$ in²

Rho = 1.67%

$f_c = 3.4$ ksi

$f_c = 3.4$ ksi

$X_o = 0.00$ in

$I_x = 27648$ in⁴

$e_u = 0.003$ in/in

$Y_o = 0.00$ in

$I_y = 27648$ in⁴

Beta1 = 0.85

Clear spacing = 3.97 in

Clear cover = 1.88 in

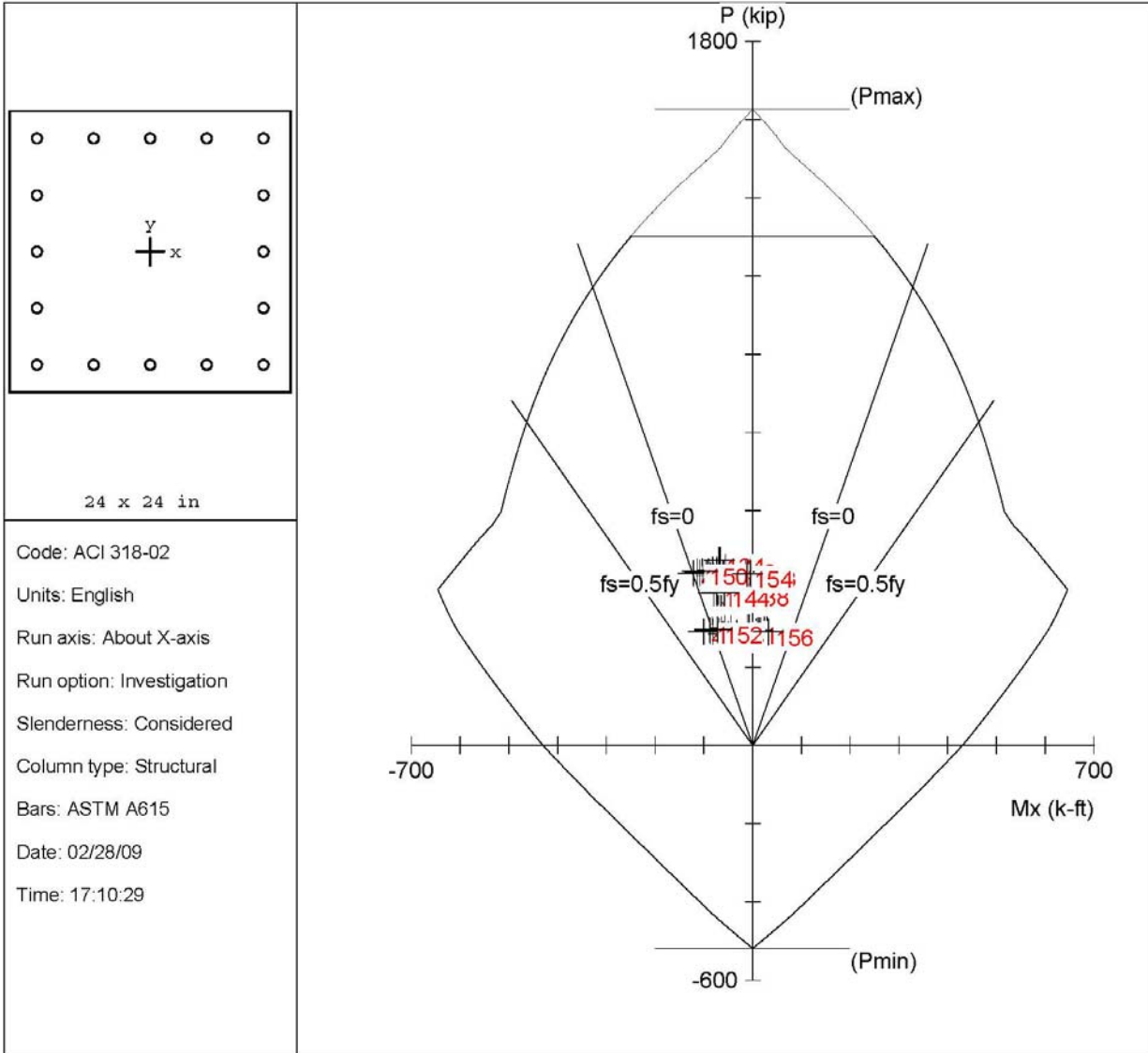
Confinement: Tied

$\phi(a) = 0.8, \phi(b) = 0.9, \phi(c) = 0.65$

$k_x(\text{braced}) = 0.94993, k_x(\text{sway}) = \text{N/A}$

Final Report

MEMBER CHECK CONTINUED: COLUMN D-7.9 FOURTH FLOOR



pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column7.9-D 5.col

Project:

Column: 7.9-D 1

Engineer:

$f_c = 4$ ksi

$f_y = 60$ ksi

$A_g = 576$ in²

16 #7 bars

$E_c = 3605$ ksi

$E_s = 29000$ ksi

$A_s = 9.60$ in²

Rho = 1.67%

$f_c = 3.4$ ksi

$f_c = 3.4$ ksi

$X_o = 0.00$ in

$I_x = 27648$ in⁴

$e_u = 0.003$ in/in

$Y_o = 0.00$ in

$I_y = 27648$ in⁴

Beta1 = 0.85

Clear spacing = 3.97 in

Clear cover = 1.88 in

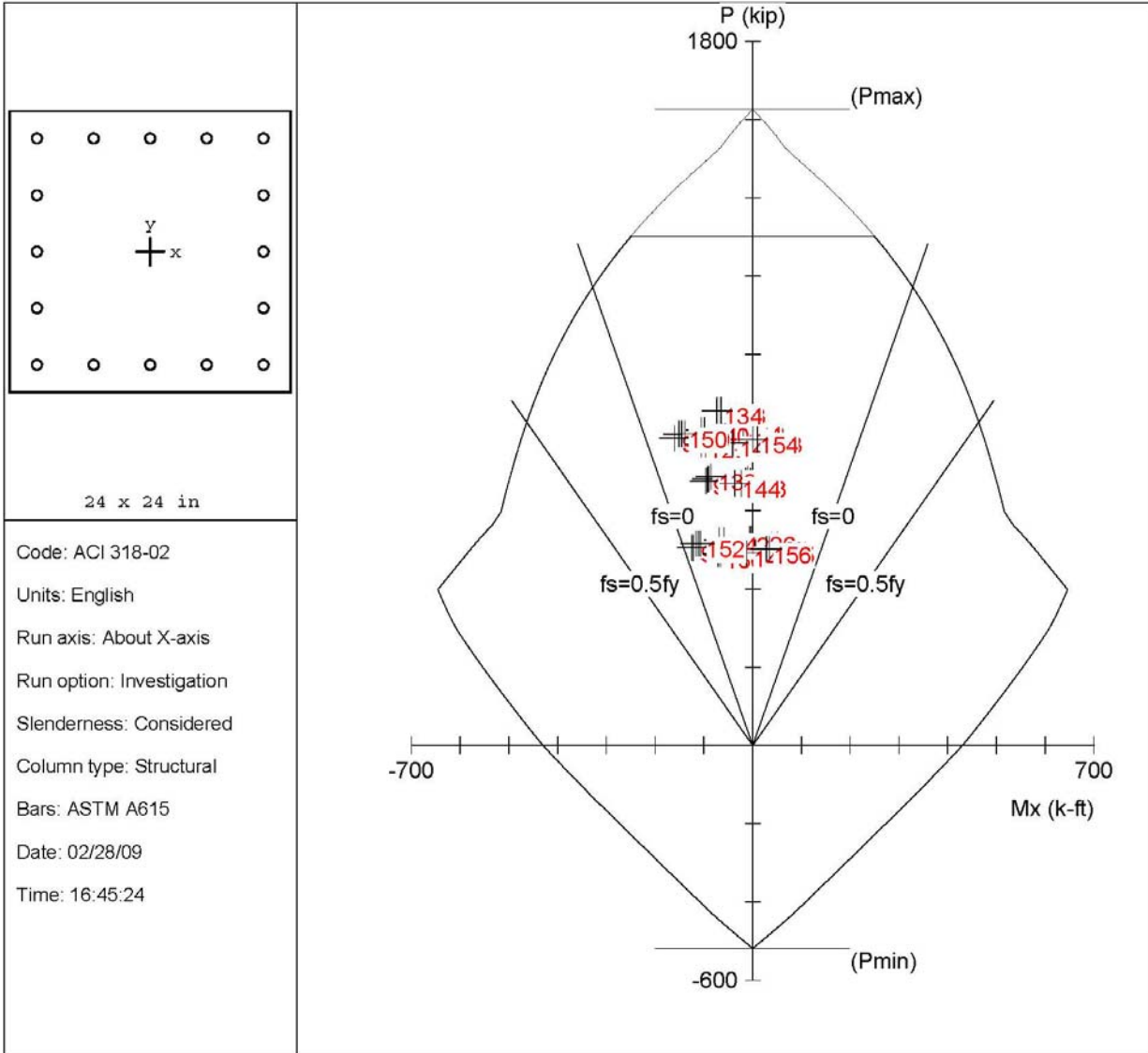
Confinement: Tied

$\phi(a) = 0.8, \phi(b) = 0.9, \phi(c) = 0.65$

$k_x(\text{braced}) = 0.96297, k_x(\text{sway}) = \text{N/A}$

Final Report

MEMBER CHECK CONTINUED: COLUMN D-7.9 THIRD FLOOR



pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column7.9-D 3.col

Project:

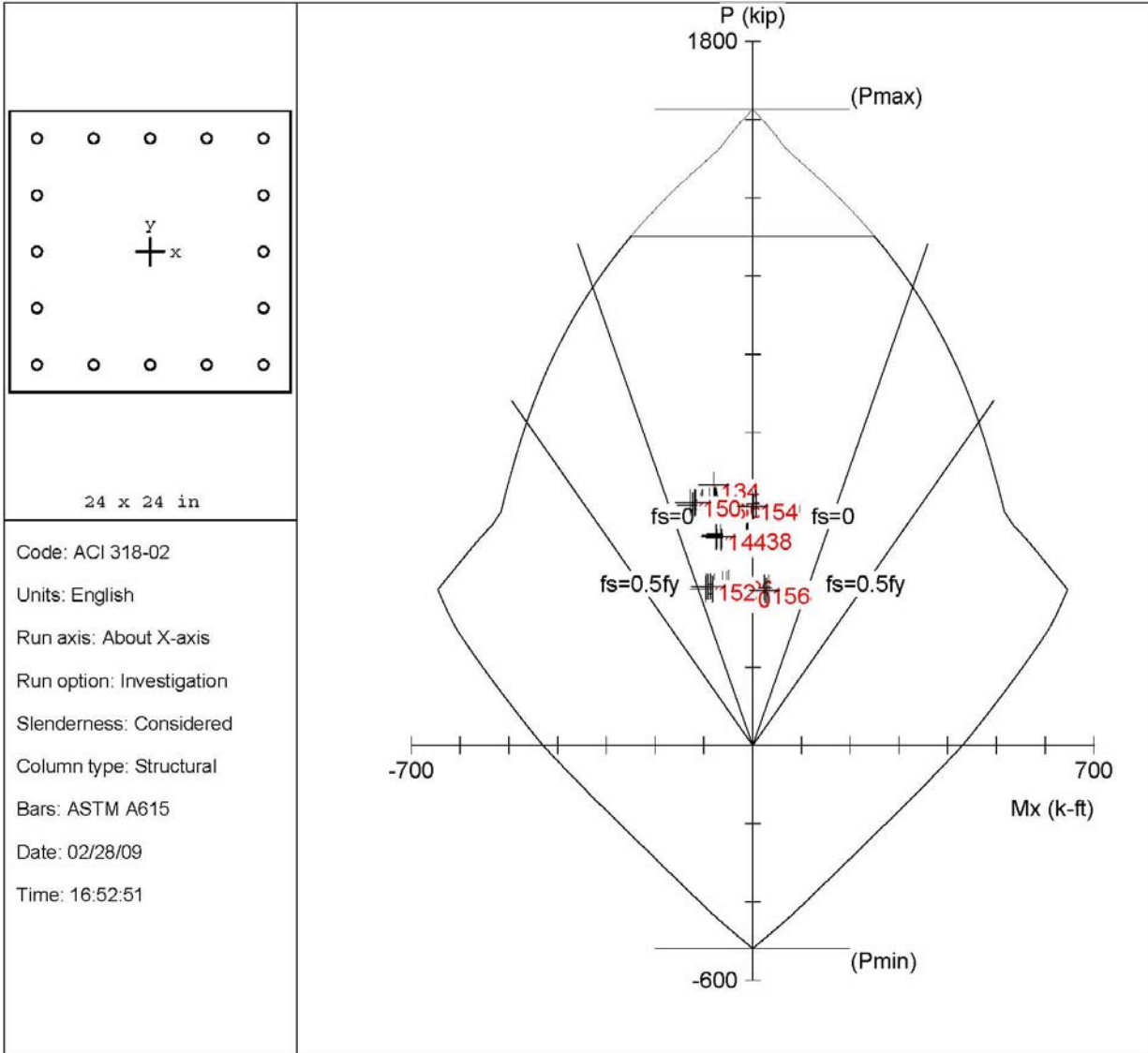
Column: 7.9-D 1

Engineer:

$f_c = 4$ ksi	$f_y = 60$ ksi	$A_g = 576$ in ²	16 #7 bars
$E_c = 3605$ ksi	$E_s = 29000$ ksi	$A_s = 9.60$ in ²	Rho = 1.67%
$f_c = 3.4$ ksi	$f_c = 3.4$ ksi	$X_o = 0.00$ in	$I_x = 27648$ in ⁴
$e_u = 0.003$ in/in		$Y_o = 0.00$ in	$I_y = 27648$ in ⁴
Beta1 = 0.85		Clear spacing = 3.97 in	Clear cover = 1.88 in
Confinement: Tied	$\phi(a) = 0.8, \phi(b) = 0.9, \phi(c) = 0.65$		
$k_x(\text{braced}) = 0.95165, k_x(\text{sway}) = \text{N/A}$			

Final Report

MEMBER CHECK CONTINUED: COLUMN D-7.9 SECOND FLOOR



24 x 24 in

Code: ACI 318-02
 Units: English
 Run axis: About X-axis
 Run option: Investigation
 Slenderness: Considered
 Column type: Structural
 Bars: ASTM A615
 Date: 02/28/09
 Time: 16:52:51

pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column7.9-D 4.col

Project:

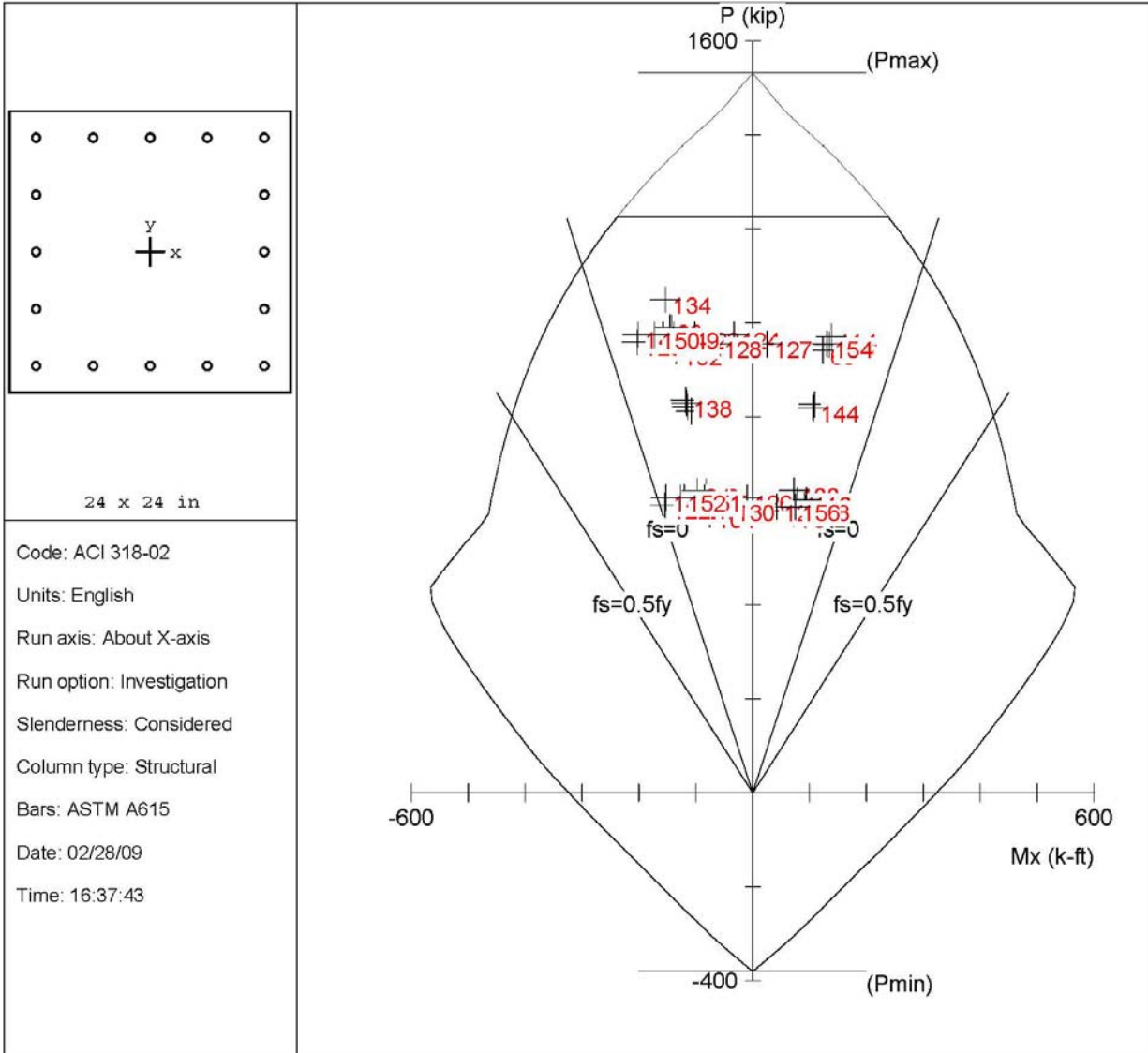
Column: 7.9-D 1

Engineer:

$f_c = 4$ ksi	$f_y = 60$ ksi	$A_g = 576$ in ²	16 #7 bars
$E_c = 3605$ ksi	$E_s = 29000$ ksi	$A_s = 9.60$ in ²	Rho = 1.67%
$f_c = 3.4$ ksi	$f_c = 3.4$ ksi	$X_o = 0.00$ in	$I_x = 27648$ in ⁴
$e_u = 0.003$ in/in		$Y_o = 0.00$ in	$I_y = 27648$ in ⁴
Beta1 = 0.85		Clear spacing = 3.97 in	Clear cover = 1.88 in
Confinement: Tied	$\phi(a) = 0.8, \phi(b) = 0.9, \phi(c) = 0.65$		
$k_x(\text{braced}) = 0.965049, k_x(\text{sway}) = \text{N/A}$			

Final Report

MEMBER CHECK CONTINUED: COLUMN D-7.9 FIRST FLOOR



pcaColumn v3.64. Licensed to: Penn State University. License ID: 52411-1010265-4-22545-28F4D

File: G:\thesis stuff\FINAL\PCA\column7.9-D 2.col

Project:

Column: 7.9-D 1

Engineer:

$f_c = 4$ ksi

$f_y = 60$ ksi

$A_g = 576$ in²

16 #6 bars

$E_c = 3605$ ksi

$E_s = 29000$ ksi

$A_s = 7.04$ in²

Rho = 1.22%

$f_c = 3.4$ ksi

$f_c = 3.4$ ksi

$X_o = 0.00$ in

$I_x = 27648$ in⁴

$e_u = 0.003$ in/in

$Y_o = 0.00$ in

$I_y = 27648$ in⁴

Beta1 = 0.85

Clear spacing = 4.13 in

Clear cover = 1.88 in

Confinement: Tied

$\phi(a) = 0.8, \phi(b) = 0.9, \phi(c) = 0.65$

$k_x(\text{braced}) = 0.94037, k_x(\text{sway}) = N/A$

Final Report

APPENDIX F: CONSTRUCTION MANAGEMENT BREADTH STUDY

Table 36: Cost Analysis Estimate for Concrete Structure with Green Roof

Detailed Cost Analysis of the Structure									
Level	Description	Amount	Material Price	Material Cost	Labor Price	Labor Cost	Equipment Price	Equipment Cost	Total Cost
Reinforcement	Foundation	58 Ton	\$935.00	\$54,230	\$430.00	\$24,940	\$30.35	\$1,760	\$80,930
	Columns	2221 Ton	\$935.00	\$2,076,635	\$430.00	\$430.00	\$30.35	\$67,407	\$2,144,472
	Beam/Slabs	572 Ton	\$935.00	\$534,820	\$430.00	\$245,960	\$30.35	\$17,360	\$798,140
	SUB-TOTAL	2851	\$935.00	\$2,665,685	\$430.00	\$430.00	\$30.35	\$86,528	\$2,752,643
Cast in Place Concrete	Foundations	6100 CY	\$109.00	\$664,900	\$14.90	\$90,890	\$5.55	\$33,855	\$789,645
	Columns	1518 CY	\$109.00	\$165,462	\$34.00	\$51,612	\$16.95	\$25,730	\$242,804
	Slabs	14192 CY	\$109.00	\$1,546,928	\$18.20	\$258,294	\$9.15	\$129,857	\$1,935,079
	Beams	8415 CY	\$109.00	\$917,235	\$26.50	\$222,998	\$1,320.00	\$11,107,800	\$12,248,033
	SUB-TOTAL	30225	\$109.00	\$3,294,525	\$23.40	\$623,794	\$1,352	\$11,297,242	\$15,215,561
Location Factor: 98.9%	Total Structure Estimate:			\$36,077,000			Total Labor Cost:		\$896,000
	Total Material Cost:			\$5,961,000			Total Equipment Cost:		\$11,384,000

Table 37: Cost Analysis Estimate for Concrete Structure, No Green Roof

Detailed Cost Analysis of the Structure-No Green Roof									
Level	Description	Amount	Material Price	Material Cost	Labor Price	Labor Cost	Equipment Price	Equipment Cost	Total Cost
Reinforcement	Foundation	58 Ton	\$935.00	\$54,230	\$430.00	\$24,940	\$30.35	\$1,760	\$80,930
	Columns	2000 Ton	\$935.00	\$1,868,972	\$430.00	\$430.00	\$30.35	\$60,667	\$1,930,068
	Beam/Slabs	544 Ton	\$935.00	\$470,642	\$430.00	\$216,445	\$30.35	\$15,277	\$702,363
	SUB-TOTAL	2560	\$935.00	\$2,393,843	\$430.00	\$430.00	\$30.35	\$77,704	\$2,471,977
Cast in Place Concrete	Foundations	6100 CY	\$109.00	\$664,900	\$14.90	\$90,890	\$5.55	\$33,855	\$789,645
	Columns	1443 CY	\$109.00	\$157,189	\$34.00	\$49,031	\$16.95	\$24,444	\$230,664
	Slabs	14192 CY	\$109.00	\$1,546,928	\$18.20	\$258,294	\$9.15	\$129,857	\$1,935,079
	Beams	7574 CY	\$109.00	\$917,235	\$26.50	\$222,998	\$1,320.00	\$11,107,800	\$12,248,033
	SUB-TOTAL	30149	\$109.00	\$3,286,252	\$23.40	\$621,213	\$1,352	\$11,295,955	\$15,203,421
Location Factor: 98.9%	Total Structure Estimate:			\$35,440,000			Total Labor Cost:		\$864,000
	Total Material Cost:			\$5,681,000			Total Equipment Cost:		\$11,374,000

Final Report

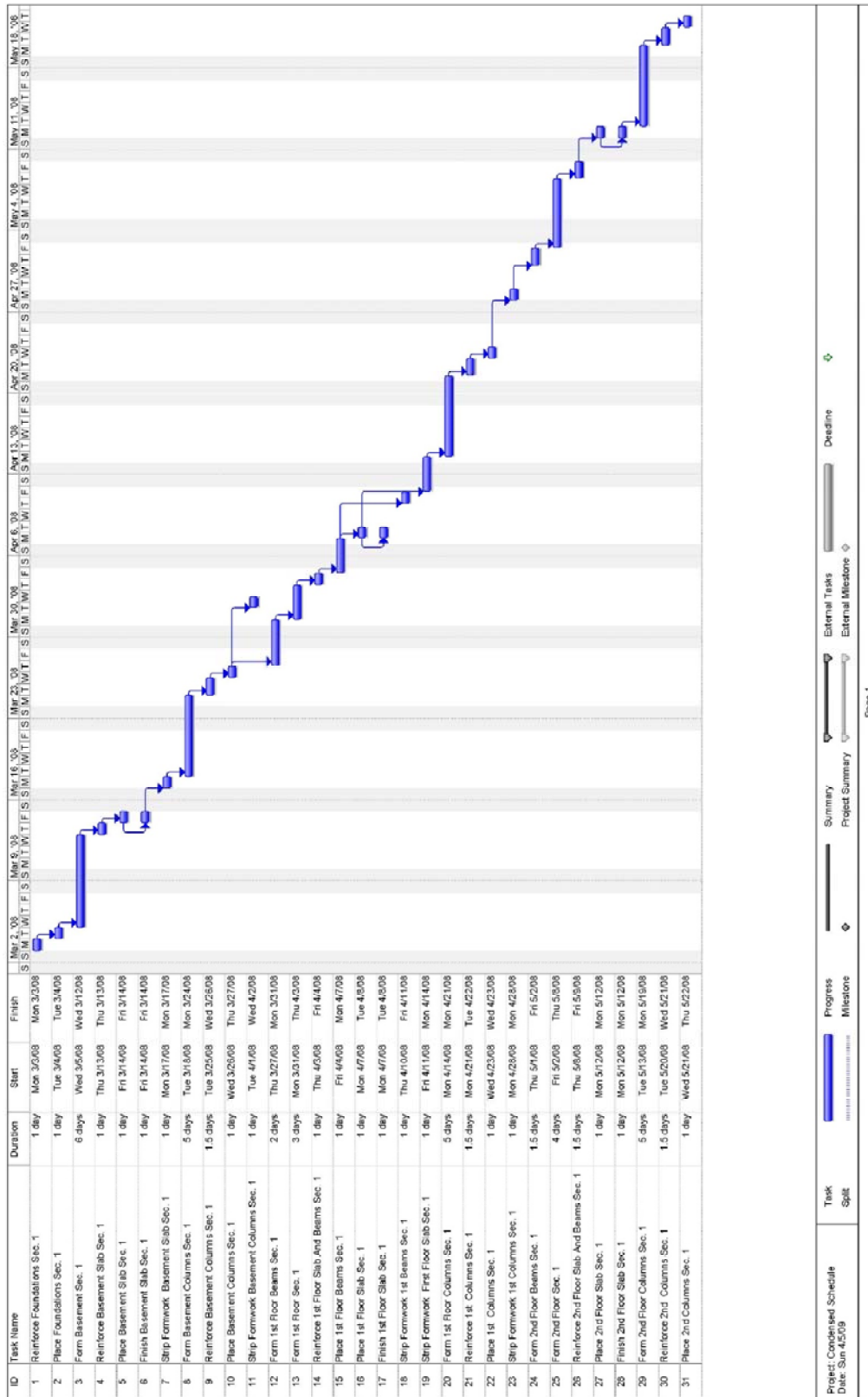


Figure 48: Condensed Gantt Chart

Final Report

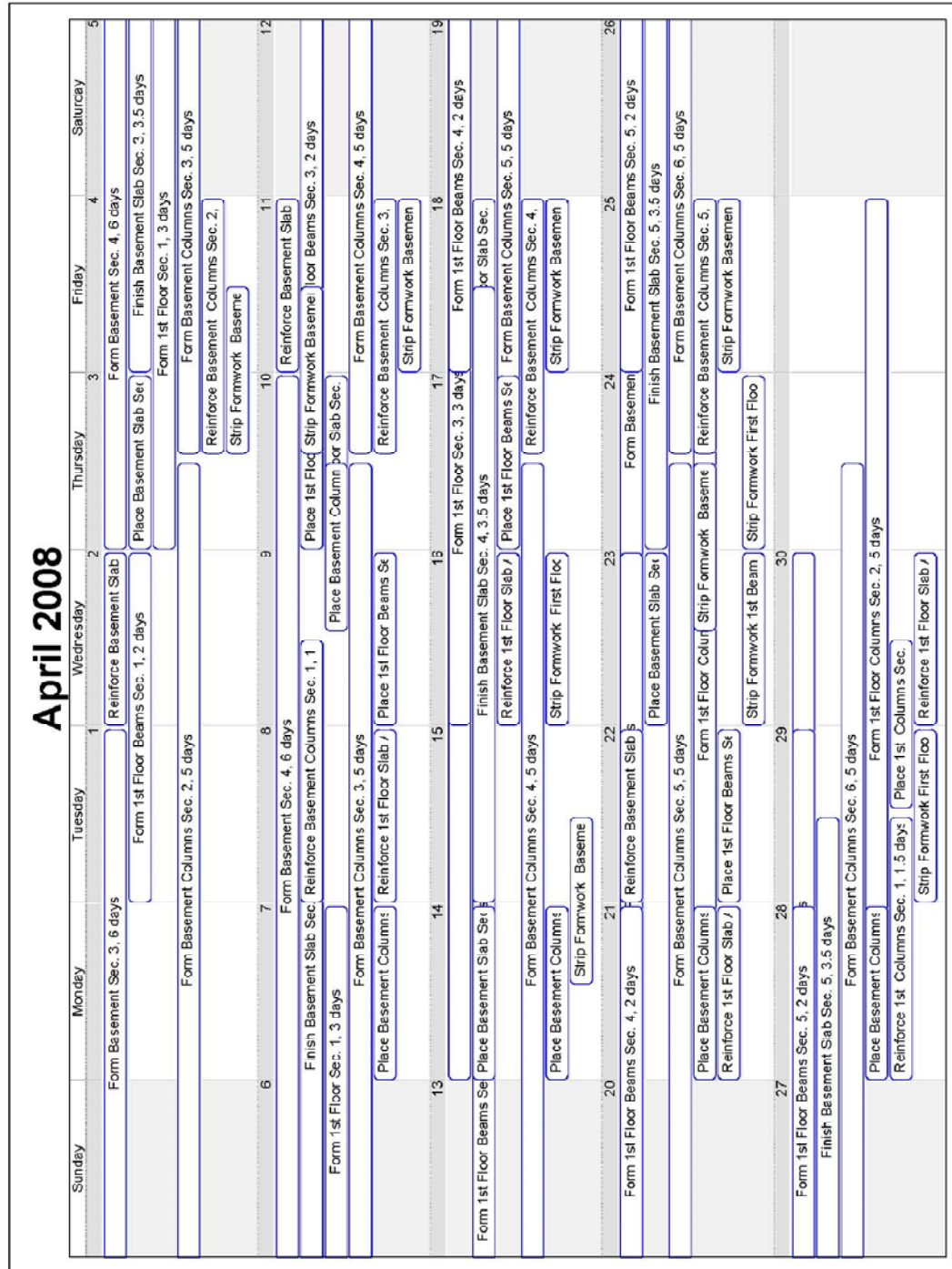


Figure 50: April Schedule Calendar

Overflow Tasks

ID	Name	Start	Finish
498	Place Basement Columns Sec. 1	Fri 4/4/08	Mon 4/7/08
490	Reinforce Basement Columns Sec. 1	Thu 4/3/08	Fri 4/4/08
573	Strip Formwork 1st Beams Sec. 1	Tue 4/15/08	Tue 4/15/08
575	Strip Formwork 1st Beams Sec. 3	Mon 4/28/08	Mon 4/28/08

Final Report

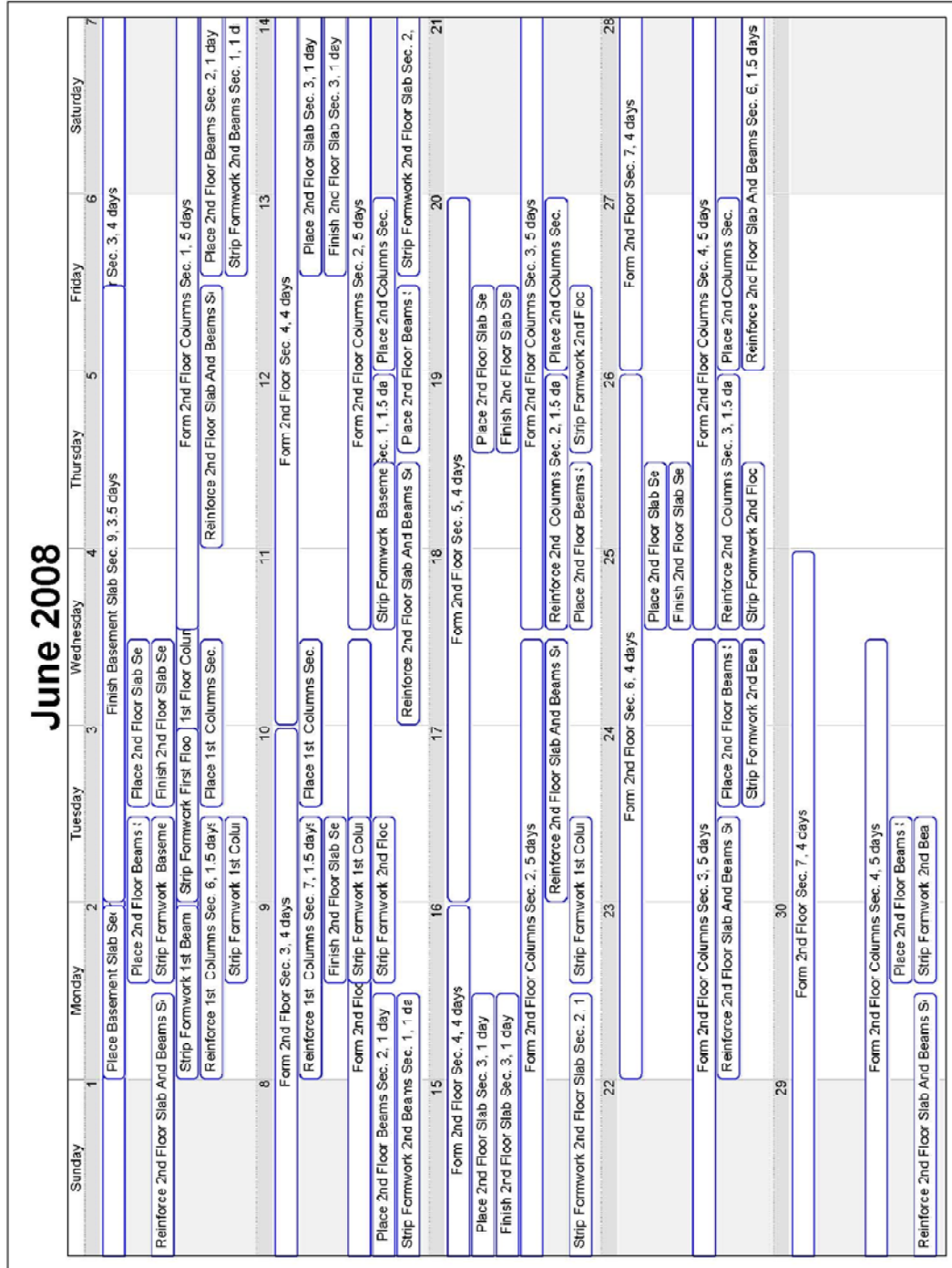


Figure 52: June Schedule Calendar

ID	Name	Start	Finish
208	Form 2nd Floor Beams Sec. 5	Mon 6/2/08	Tue 6/3/08
584	Strip Formwork 2nd Beams Sec. 2	Thu 6/12/08	Fri 6/13/08
209	Form 2nd Floor Beams Sec. 6	Mon 6/9/08	Tue 6/10/08
585	Strip Formwork 2nd Beams Sec. 3	Wed 6/18/08	Thu 6/19/08
645	Strip Formwork 2nd Columns Sec. 1	Thu 6/19/08	Thu 6/19/08
210	Form 2nd Floor Beams Sec. 7	Mon 6/16/08	Tue 6/17/08
211	Form 3rd Floor Beams Sec. 1	Thu 6/19/08	Fri 6/20/08
646	Strip Formwork 2nd Columns Sec. 2	Thu 6/26/08	Thu 6/26/08
212	Form 3rd Floor Beams Sec. 2	Thu 6/26/08	Fri 6/27/08
213	Form 3rd Floor Beams Sec. 3	Fri 6/27/08	Mon 6/30/08

Final Report

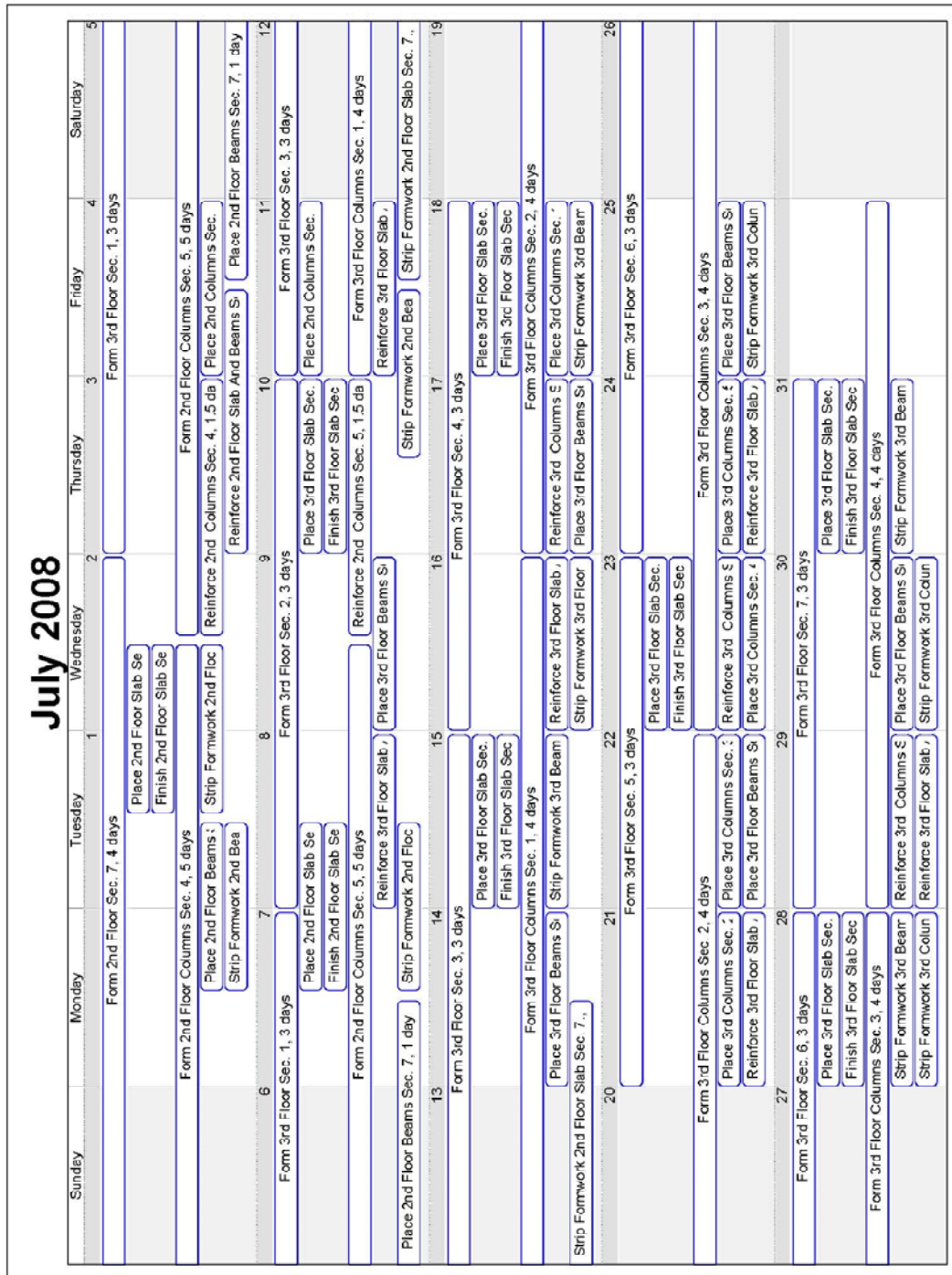


Figure 53: July Schedule Calendar

Final Report

JULY OVERFLOW TASKS

Overflow Tasks				
ID	Name		Start	Finish
588	Strip Formwork 2nd Beams Sec. 6		Fri 7/4/08	Mon 7/7/08
647	Strip Formwork 2nd Columns Sec. 3		Thu 7/3/08	Thu 7/3/08
214	Form 3rd Floor Beams Sec. 4		Thu 7/3/08	Fri 7/4/08
215	Form 3rd Floor Beams Sec. 5		Fri 7/4/08	Mon 7/7/08
648	Strip Formwork 2nd Columns Sec. 4		Thu 7/10/08	Thu 7/10/08
216	Form 3rd Floor Beams Sec. 6		Thu 7/10/08	Fri 7/11/08
217	Form 3rd Floor Beams Sec. 7		Fri 7/11/08	Mon 7/14/08
649	Strip Formwork 2nd Columns Sec. 5		Thu 7/17/08	Thu 7/17/08
218	Form 3rd Floor Beams Sec. 8		Thu 7/17/08	Fri 7/18/08
219	Form 3rd Floor Beams Sec. 9		Fri 7/18/08	Mon 7/21/08
535	Strip Formwork 3rd Floor Slab Sec. 2		Mon 7/21/08	Mon 7/21/08
536	Strip Formwork 3rd Floor Slab Sec. 3		Thu 7/24/08	Thu 7/24/08
593	Strip Formwork 3rd Beams Sec. 3		Wed 7/23/08	Wed 7/23/08
651	Strip Formwork 3rd Columns Sec. 1		Thu 7/24/08	Thu 7/24/08
220	Form 4th Floor Beams Sec. 1		Tue 7/22/08	Wed 7/23/08
221	Form 4th Floor Beams Sec. 2		Thu 7/24/08	Fri 7/25/08
537	Strip Formwork 3rd Floor Slab Sec. 4		Tue 7/29/08	Tue 7/29/08
654	Strip Formwork 3rd Columns Sec. 4		Tue 7/29/08	Tue 7/29/08
222	Form 4th Floor Beams Sec. 3		Mon 7/28/08	Tue 7/29/08
223	Form 4th Floor Beams Sec. 4		Wed 7/30/08	Thu 7/31/08

AUGUST OVERFLOW TASKS

Overflow Tasks				
ID	Name		Start	Finish
538	Strip Formwork 3rd Floor Slab Sec. 5		Fri 8/1/08	Fri 8/1/08
224	Form 4th Floor Beams Sec. 5		Fri 8/1/08	Mon 8/4/08
468	Place 3rd Floor Beams Sec. 7		Mon 8/4/08	Mon 8/4/08
539	Strip Formwork 3rd Floor Slab Sec. 6		Wed 8/6/08	Wed 8/6/08
225	Form 4th Floor Beams Sec. 6		Tue 8/5/08	Wed 8/6/08
226	Form 4th Floor Beams Sec. 7		Thu 8/7/08	Fri 8/8/08
227	Form 5th Floor Beams Sec. 1		Mon 8/11/08	Tue 8/12/08
228	Form 5th Floor Beams Sec. 2		Wed 8/13/08	Thu 8/14/08
229	Form 5th Floor Beams Sec. 3		Fri 8/15/08	Mon 8/18/08
230	Form 5th Floor Beams Sec. 4		Tue 8/19/08	Wed 8/20/08
231	Form 5th Floor Beams Sec. 5		Thu 8/21/08	Fri 8/22/08
232	Form 5th Floor Beams Sec. 6		Mon 8/25/08	Tue 8/26/08
233	Form 5th Floor Beams Sec. 7		Wed 8/27/08	Thu 8/28/08
234	Form Roof Beams Sec. 1		Fri 8/29/08	Mon 9/1/08

Final Report

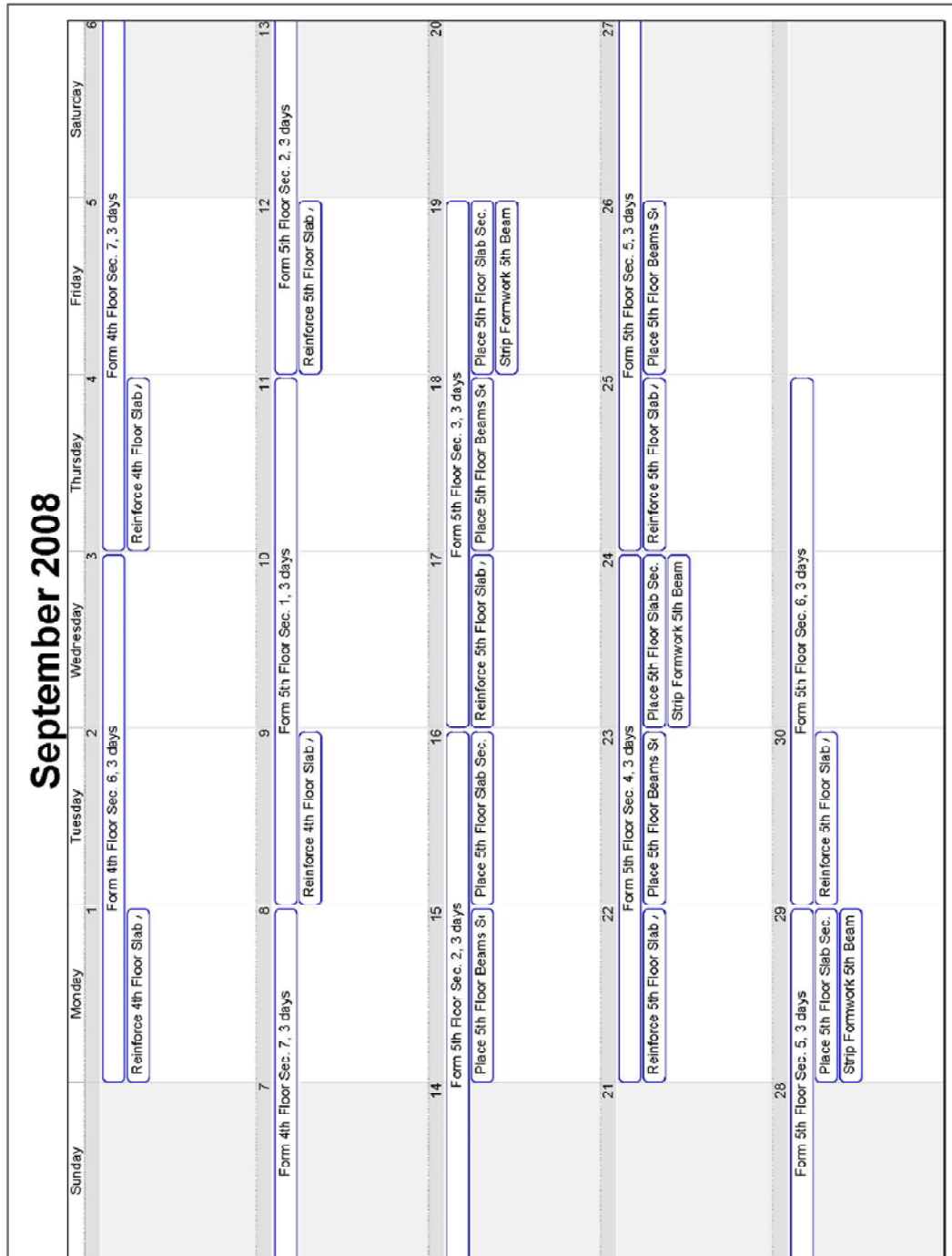


Figure 55: September Schedule Calendar

ID	Name	Start	Finish
234	Form Roof Beams Sec. 1	Fri 8/29/08	Mon 9/1/08
235	Form Roof Beams Sec. 2	Mon 9/1/08	Tue 9/2/08
236	Form Roof Beams Sec. 3	Wed 9/3/08	Thu 9/4/08
237	Form Roof Beams Sec. 4	Thu 9/4/08	Fri 9/5/08
238	Form Roof Beams Sec. 5	Mon 9/8/08	Tue 9/9/08
239	Form Roof Beams Sec. 6	Tue 9/9/08	Wed 9/10/08
240	Form Roof Beams Sec. 7	Thu 9/11/08	Fri 9/12/08
241	Form Penthouse Beams Sec. 1	Fri 9/12/08	Tue 9/16/08
242	Form Penthouse Beams Sec. 2	Tue 9/16/08	Thu 9/18/08
243	Form Penthouse Beams Sec. 3	Thu 9/18/08	Mon 9/22/08
244	Form Penthouse Beams Sec. 4	Mon 9/22/08	Wed 9/24/08

Final Report

OCTOBER OVERFLOW TASKS

Overflow Tasks

ID	Name	Start	Finish
439	Place Roof Beams Sec. 2	Wed 10/15/08	Wed 10/15/08
456	Place 4th Floor Beams Sec. 3	Mon 10/13/08	Mon 10/13/08
457	Place 4th Floor Beams Sec. 4	Tue 10/14/08	Tue 10/14/08
458	Place 4th Floor Beams Sec. 5	Wed 10/15/08	Wed 10/15/08
459	Place 4th Floor Beams Sec. 6	Thu 10/16/08	Thu 10/16/08
460	Place 4th Floor Beams Sec. 7	Fri 10/17/08	Fri 10/17/08
422	Reinforce Roof Slab And Beams Sec. 3	Thu 10/16/08	Fri 10/17/08
544	Strip Formwork 4th Floor Slab Sec. 1	Thu 10/16/08	Thu 10/16/08
545	Strip Formwork 4th Floor Slab Sec. 2	Fri 10/17/08	Fri 10/17/08
601	Strip Formwork 4th Beams Sec. 1	Wed 10/15/08	Wed 10/15/08
602	Strip Formwork 4th Beams Sec. 2	Thu 10/16/08	Thu 10/16/08
603	Strip Formwork 4th Beams Sec. 3	Fri 10/17/08	Fri 10/17/08
615	Strip Formwork 5th Beams Sec. 7	Wed 10/15/08	Wed 10/15/08
617	Strip Formwork Roof Beams Sec. 1	Thu 10/16/08	Thu 10/16/08
331	Form 5th Floor Columns Sec. 1	Wed 10/22/08	Thu 10/30/08
423	Reinforce Roof Slab And Beams Sec. 4	Tue 10/21/08	Wed 10/22/08
424	Reinforce Roof Slab And Beams Sec. 5	Fri 10/24/08	Mon 10/27/08
440	Place Roof Beams Sec. 3	Mon 10/20/08	Mon 10/20/08
441	Place Roof Beams Sec. 4	Thu 10/23/08	Thu 10/23/08
546	Strip Formwork 4th Floor Slab Sec. 3	Mon 10/20/08	Mon 10/20/08
547	Strip Formwork 4th Floor Slab Sec. 4	Tue 10/21/08	Tue 10/21/08
548	Strip Formwork 4th Floor Slab Sec. 5	Wed 10/22/08	Wed 10/22/08
549	Strip Formwork 4th Floor Slab Sec. 6	Thu 10/23/08	Thu 10/23/08
550	Strip Formwork 4th Floor Slab Sec. 7	Fri 10/24/08	Fri 10/24/08
604	Strip Formwork 4th Beams Sec. 4	Mon 10/20/08	Mon 10/20/08
605	Strip Formwork 4th Beams Sec. 5	Tue 10/21/08	Tue 10/21/08
606	Strip Formwork 4th Beams Sec. 6	Wed 10/22/08	Wed 10/22/08
607	Strip Formwork 4th Beams Sec. 7	Thu 10/23/08	Thu 10/23/08
618	Strip Formwork Roof Beams Sec. 2	Tue 10/21/08	Tue 10/21/08
619	Strip Formwork Roof Beams Sec. 3	Fri 10/24/08	Fri 10/24/08
657	Strip Formwork 4th Columns Sec. 1	Fri 10/24/08	Fri 10/24/08
346	Form Roof Columns Sec. 1	Fri 10/31/08	Wed 11/5/08
425	Reinforce Roof Slab And Beams Sec. 6	Wed 10/29/08	Thu 10/30/08
442	Place Roof Beams Sec. 5	Tue 10/28/08	Tue 10/28/08
443	Place Roof Beams Sec. 6	Fri 10/31/08	Fri 10/31/08
552	Strip Formwork 5th Floor Slab Sec. 1	Mon 10/27/08	Mon 10/27/08
553	Strip Formwork 5th Floor Slab Sec. 2	Tue 10/28/08	Tue 10/28/08
554	Strip Formwork 5th Floor Slab Sec. 3	Wed 10/29/08	Wed 10/29/08
555	Strip Formwork 5th Floor Slab Sec. 4	Thu 10/30/08	Thu 10/30/08
556	Strip Formwork 5th Floor Slab Sec. 5	Fri 10/31/08	Fri 10/31/08
620	Strip Formwork Roof Beams Sec. 4	Wed 10/29/08	Wed 10/29/08
658	Strip Formwork 4th Columns Sec. 2	Mon 10/27/08	Mon 10/27/08
659	Strip Formwork 4th Columns Sec. 3	Tue 10/28/08	Tue 10/28/08
661	Strip Formwork 4th Columns Sec. 5	Thu 10/30/08	Thu 10/30/08
660	Strip Formwork 4th Columns Sec. 4	Wed 10/29/08	Wed 10/29/08

Final Report

NOVEMBER OVERFLOW TASKS

ID	Name	Overflow Tasks	Start	Finish
346	Form Roof Columns Sec. 1		Fri 10/31/08	Wed 11/5/08
347	Form Roof Columns Sec. 2		Wed 11/5/08	Mon 11/10/08
341	Place 5th Columns Sec. 1		Mon 11/3/08	Mon 11/3/08
352	Reinforce Roof Columns Sec. 1		Wed 11/5/08	Thu 11/6/08
358	Place Roof Columns Sec. 1		Thu 11/6/08	Fri 11/7/08
426	Reinforce Roof Slab And Beams Sec. 7		Mon 11/3/08	Tue 11/4/08
428	Reinforce Pent Slab And Beams Sec. 1		Wed 11/5/08	Thu 11/6/08
429	Reinforce Pent Slab And Beams Sec. 2		Fri 11/7/08	Mon 11/10/08
433	Place Penthouse Beams Sec. 1		Thu 11/6/08	Fri 11/7/08
444	Place Roof Beams Sec. 7		Wed 11/5/08	Wed 11/5/08
557	Strip Formwork 5th Floor Slab Sec. 6		Mon 11/3/08	Mon 11/3/08
558	Strip Formwork 5th Floor Slab Sec. 7.		Tue 11/4/08	Tue 11/4/08
560	Strip Formwork Roof Slab Sec. 1		Wed 11/5/08	Wed 11/5/08
561	Strip Formwork Roof Slab Sec. 2		Thu 11/6/08	Thu 11/6/08
562	Strip Formwork Roof Slab Sec. 3		Fri 11/7/08	Fri 11/7/08
621	Strip Formwork Roof Beams Sec. 5		Mon 11/3/08	Mon 11/3/08
663	Strip Formwork 5th Columns Sec. 1		Fri 11/7/08	Fri 11/7/08
622	Strip Formwork Roof Beams Sec. 6		Thu 11/6/08	Thu 11/6/08
348	Form Roof Columns Sec. 3		Tue 11/11/08	Fri 11/14/08
354	Reinforce Roof Columns Sec. 3		Fri 11/14/08	Mon 11/17/08
364	Form Penthouse Columns Sec. 1		Tue 11/11/08	Mon 11/17/08
353	Reinforce Roof Columns Sec. 2		Tue 11/11/08	Tue 11/11/08
359	Place Roof Columns Sec. 2		Wed 11/12/08	Wed 11/12/08
430	Reinforce Pent Slab And Beams Sec. 3		Tue 11/11/08	Wed 11/12/08
431	Reinforce Pent Slab And Beams Sec. 4		Thu 11/13/08	Fri 11/14/08
436	Place Penthouse Beams Sec. 4		Fri 11/14/08	Mon 11/17/08
434	Place Penthouse Beams Sec. 2		Mon 11/10/08	Tue 11/11/08
435	Place Penthouse Beams Sec. 3		Wed 11/12/08	Thu 11/13/08
568	Strip Formwork Penthouse Slab Sec. 1		Fri 11/14/08	Fri 11/14/08
563	Strip Formwork Roof Slab Sec. 4		Mon 11/10/08	Mon 11/10/08
564	Strip Formwork Roof Slab Sec. 5		Tue 11/11/08	Tue 11/11/08
565	Strip Formwork Roof Slab Sec. 6		Wed 11/12/08	Wed 11/12/08
566	Strip Formwork Roof Slab Sec. 7.		Thu 11/13/08	Thu 11/13/08
623	Strip Formwork Roof Beams Sec. 7		Tue 11/11/08	Tue 11/11/08
626	Strip Formwork Penthouse Beams Sec. 2		Thu 11/13/08	Fri 11/14/08
625	Strip Formwork Penthouse Beams Sec. 1		Tue 11/11/08	Wed 11/12/08
668	Strip Formwork Roof Columns Sec. 1		Wed 11/12/08	Thu 11/13/08
355	Reinforce Roof Columns Sec. 4		Thu 11/20/08	Thu 11/20/08
360	Place Roof Columns Sec. 3		Mon 11/17/08	Tue 11/18/08
361	Place Roof Columns Sec. 4		Fri 11/21/08	Fri 11/21/08
365	Form Penthouse Columns Sec. 2		Tue 11/18/08	Mon 11/24/08
372	Place Penthouse Columns Sec. 1		Wed 11/19/08	Wed 11/19/08
368	Reinforce Penthouse Columns Sec. 1		Tue 11/18/08	Tue 11/18/08
570	Strip Formwork Penthouse Slab Sec. 3		Wed 11/19/08	Thu 11/20/08
571	Strip Formwork Penthouse Slab Sec. 4		Fri 11/21/08	Mon 11/24/08
569	Strip Formwork Penthouse Slab Sec. 2		Mon 11/17/08	Tue 11/18/08
628	Strip Formwork Penthouse Beams Sec. 4		Wed 11/19/08	Thu 11/20/08
670	Strip Formwork Roof Columns Sec. 3		Fri 11/21/08	Mon 11/24/08
627	Strip Formwork Penthouse Beams Sec. 3		Mon 11/17/08	Tue 11/18/08
664	Strip Formwork 5th Columns Sec. 2		Tue 11/18/08	Tue 11/18/08
669	Strip Formwork Roof Columns Sec. 2		Tue 11/18/08	Tue 11/18/08
665	Strip Formwork 5th Columns Sec. 3		Thu 11/27/08	Thu 11/27/08
671	Strip Formwork Roof Columns Sec. 4		Thu 11/27/08	Thu 11/27/08
674	Strip Formwork Penthouse Columns Sec. 1		Tue 11/25/08	Tue 11/25/08

Final Report

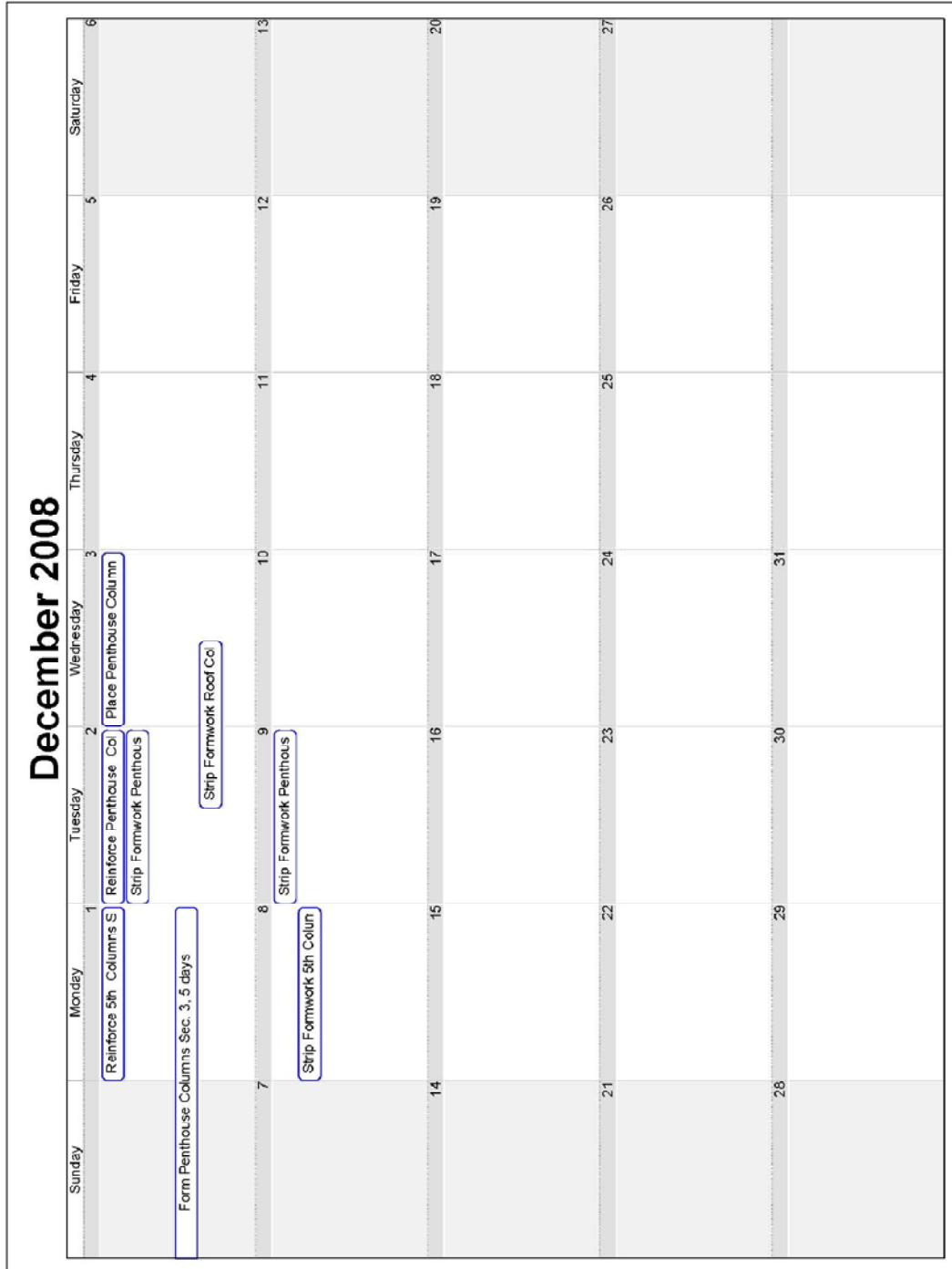


Figure 58: December Schedule Calendar

Final Report

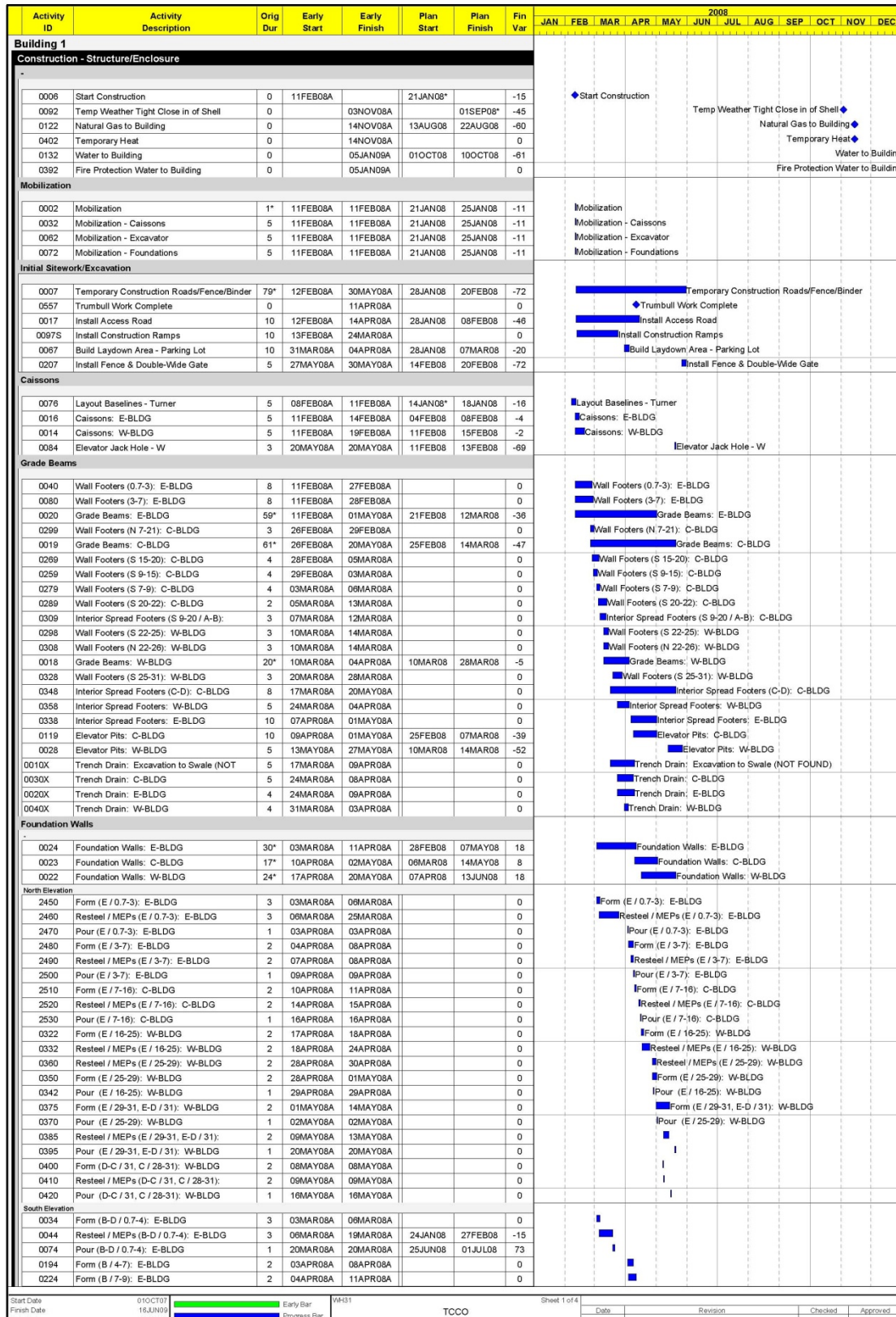


Figure 59: Turner Construction Schedule 1/4

Final Report

APPENDIX G: SUSTAINABLE ARCHITECTURE BREADTH STUDY



**LEED for New Construction v 2.2
 Registered Project Checklist**

Project Name: Westinghouse Electric Company Corporate Headquarters

Project Address: 1000 Westinghouse Drive, Cranberry Township, PA 16066

Yes	?	No				
28	5	33	Project Totals (Pre-Certification Estimates)			69 Points
CERTIFIED			Certified: 26-32 points	Silver: 33-38 points	Gold: 39-51 points	Platinum: 52-69 points

Yes	?	No		
8	3	3	Sustainable Sites	14 Points

Yes	?	No		
1	0	0	Prereq 1	Construction Activity Pollution Prevention Required
0	0	1	Credit 1	Site Selection 1
0	0	1	Credit 2	Development Density & Community Connectivity 1
1	0	0	Credit 3	Brownfield Redevelopment 1
1	0	0	Credit 4.1	Alternative Transportation , Public Transportation 1
1	0	0	Credit 4.2	Alternative Transportation , Bicycle Storage & Changing Rooms 1
0	0	1	Credit 4.3	Alternative Transportation , Low-Emitting & Fuel Efficient Vehicles 1
1	0	0	Credit 4.4	Alternative Transportation , Parking Capacity 1
1	0	0	Credit 5.1	Site Development , Protect or Restore Habitat 1
1	0	0	Credit 5.2	Site Development , Maximize Open Space 1
1	0	0	Credit 6.1	Stormwater Design , Quantity Control 1
	1		Credit 6.2	Stormwater Design , Quality Control 1
	1		Credit 7.1	Heat Island Effect , Non-Roof 1
1	0	0	Credit 7.2	Heat Island Effect , Roof 1
	1		Credit 8	Light Pollution Reduction 1

Yes	?	No		
2	0	0	Water Efficiency	5 Points

1	0	0	Credit 1.1	Water Efficient Landscaping , Reduce by 50% 1
1	0	0	Credit 1.2	Water Efficient Landscaping , No Potable Use or No Irrigation 1
			Credit 2	Innovative Wastewater Technologies 1
			Credit 3.1	Water Use Reduction , 20% Reduction 1
			Credit 3.2	Water Use Reduction , 30% Reduction 1

Figure 63: LEED Checklist from <http://www.usgbc.org/showfile.aspx?documentid=3998> 1/4

Final Report



LEED for New Construction v 2.2
 Registered Project Checklist

Yes	?	No			
2	0	15	Energy & Atmosphere		17 Points
Yes			Prereq 1	Fundamental Commissioning of the Building Energy Systems	Required
Yes			Prereq 1	Minimum Energy Performance	Required
Yes			Prereq 1	Fundamental Refrigerant Management	Required
*Note for EAc1: All LEED for New Construction projects registered after June 26, 2007 are required to achieve at least two (2) points.					
2	0	8	Credit 1	Optimize Energy Performance	1 to 10
				Credit 1.1 10.5% New Buildings / 3.5% Existing Building Renovations	1
			-->	Credit 1.2 14% New Buildings / 7% Existing Building Renovations	2
				Credit 1.3 17.5% New Buildings / 10.5% Existing Building Renovations	3
				Credit 1.4 21% New Buildings / 14% Existing Building Renovations	4
				Credit 1.5 24.5% New Buildings / 17.5% Existing Building Renovations	5
				Credit 1.6 28% New Buildings / 21% Existing Building Renovations	6
				Credit 1.7 31.5% New Buildings / 24.5% Existing Building Renovations	7
				Credit 1.8 35% New Buildings / 28% Existing Building Renovations	8
				Credit 1.9 38.5% New Buildings / 31.5% Existing Building Renovations	9
				Credit 1.10 42% New Buildings / 35% Existing Building Renovations	10
0	0	3	Credit 2	On-Site Renewable Energy	1 to 3
				Credit 2.1 2.5% Renewable Energy	1
				Credit 2.2 7.5% Renewable Energy	2
				Credit 2.3 12.5% Renewable Energy	3
0	0	1	Credit 3	Enhanced Commissioning	1
0	0	1	Credit 4	Enhanced Refrigerant Management	1
0	0	1	Credit 5	Measurement & Verification	1
0	0	1	Credit 6	Green Power	1

Figure 64: LEED Checklist from <http://www.usgbc.org/showfile.aspx?documentid=3998> 2/4

Final Report



LEED for New Construction v 2.2
 Registered Project Checklist

Yes	?	No			
5	0	8	Materials & Resources		13 Points

Yes	?	No	Prereq	Requirement	Points
0	0	1	Prereq 1	Storage & Collection of Recyclables	Required
0	0	1	Credit 1.1	Building Reuse , Maintain 75% of Existing Walls, Floors & Roof	1
0	0	1	Credit 1.2	Building Reuse , Maintain 95% of Existing Walls, Floors & Roof	1
0	0	1	Credit 1.3	Building Reuse , Maintain 50% of Interior Non-Structural Elements	1
1	0	0	Credit 2.1	Construction Waste Management , Divert 50% from Disposal	1
0	0	1	Credit 2.2	Construction Waste Management , Divert 75% from Disposal	1
1	0	0	Credit 3.1	Materials Reuse , 5%	1
1	0	0	Credit 3.2	Materials Reuse , 10%	1
0	0	1	Credit 4.1	Recycled Content , 10% (post-consumer + 1/2 pre-consumer)	1
0	0	1	Credit 4.2	Recycled Content , 20% (post-consumer + 1/2 pre-consumer)	1
1	0	0	Credit 5.1	Regional Materials , 10% Extracted, Processed & Manufactured	1
1	0	0	Credit 5.2	Regional Materials , 20% Extracted, Processed & Manufactured	1
0	0	1	Credit 6	Rapidly Renewable Materials	1
0	0	1	Credit 7	Certified Wood	1

Yes	?	No			
10	2	3	Indoor Environmental Quality		15 Points

Yes	?	No	Prereq	Requirement	Points
1	0	0	Prereq 1	Minimum IAQ Performance	Required
1	0	0	Prereq 2	Environmental Tobacco Smoke (ETS) Control	Required
1	0	0	Credit 1	Outdoor Air Delivery Monitoring	1
1	0	0	Credit 2	Increased Ventilation	1
1	1	0	Credit 3.1	Construction IAQ Management Plan , During Construction	1
1	1	0	Credit 3.2	Construction IAQ Management Plan , Before Occupancy	1
1	0	0	Credit 4.1	Low-Emitting Materials , Adhesives & Sealants	1
1	0	0	Credit 4.2	Low-Emitting Materials , Paints & Coatings	1
1	0	0	Credit 4.3	Low-Emitting Materials , Carpet Systems	1
0	0	1	Credit 4.4	Low-Emitting Materials , Composite Wood & Agrifiber Products	1
0	0	1	Credit 5	Indoor Chemical & Pollutant Source Control	1
1	0	0	Credit 6.1	Controllability of Systems , Lighting	1
1	0	0	Credit 6.2	Controllability of Systems , Thermal Comfort	1
1	0	0	Credit 7.1	Thermal Comfort , Design	1
1	0	0	Credit 7.2	Thermal Comfort , Verification	1
1	0	0	Credit 8.1	Daylight & Views , Daylight 75% of Spaces	1
0	0	1	Credit 8.2	Daylight & Views , Views for 90% of Spaces	1

Figure 65: LEED Checklist from <http://www.usgbc.org/showfile.aspx?documentid=3998> 3/4

Final Report



LEED for New Construction v 2.2
 Registered Project Checklist

Yes	?	No		
1	0	4	Innovation & Design Process	5 Points
0	0	1	Credit 1.1 Innovation in Design: Provide Specific Title	1
0	0	1	Credit 1.2 Innovation in Design: Provide Specific Title	1
0	0	1	Credit 1.3 Innovation in Design: Provide Specific Title	1
0	0	1	Credit 1.4 Innovation in Design: Provide Specific Title	1
1	0	0	Credit 2 LEED® Accredited Professional	1

Figure 66: LEED Checklist from <http://www.usgbc.org/showfile.aspx?documentid=3998> 4/4

APPENDIX H: REFERENCES

- American Concrete Institute. ACI 318-08: Building Code Requirements for Structural Concrete. ACI: Farmington Hills, MI, 2008.
- American Society of Civil Engineers. ASCE 7-05: Minimum Design Loads for Building and Other Structures. ASCE: Reston, VA, 2006.
- Audubon Society of Western Pennsylvania. "Culture and Use Guide For Western Pennsylvania Native Plants." ACNP Culture and Use Guide. 2008. Audubon Society of Western Pennsylvania. 16 Jan. 2009
<http://www.aswp.org/acnp_culture_and_use_guide.html>
- CCW 500R Green Roof Waterproofing System. 10 Mar. 2009. Carlisle Coatings and Waterproofing. 24 Mar. 2009
<www.carlisle-ccw.com/Doco/spec07555613CCW500RGreenRoofWaterproofingSystem.pdf>.
- International Code Council. International Building Code 2006. ICC: New York, NY, 2006.
- Local Native Plant Species Allegheny County Area. Audubon Society of Western Pennsylvania. 3 Apr. 2009
<http://www.aswp.org/files/allegheny_county_pennsylvania_native_plants_aswp.pdf>.
- Roof Drain Calculator. Portal Plus. 29 Mar. 2009 <http://www.portalsplus.com/drain_calc.htm>.
- RSMeans Construction Publishers and Consultants. Building Construction Cost Data 2008 66th Annual Edition. Reed Construction Data, Inc.: Kingston, MA, 2007.
- Steel Construction Manual. 13th ed. American Institute of Steel Construction. AISC, 2005
- U.S. Green Building Council. LEED for New Construction and Major Renovations. Oct. 2005. U.S.G.B.C. 26 Mar. 2009 <<http://www.usgbc.org/showfile.aspx?documentid=1095>>.
- U.S. Green Building Council. LEED For New Construction v 2.2 Registered Project Checklist. May 2008. U.S.G.B.C. 26 Mar. 2009 <<http://www.usgbc.org/showfile.aspx?documentid=3998>>.
- What are green roofs? June 2008. Department of Energy Quality Michigan. 17 Jan. 2009
<www.deq.state.mi.us/documents/deq-ess-p2-p2week-greenroofresources.doc>.